



October 27, 2023

Mr. Ron Ellis
Region D Project Manager
Texas Water Development Board
P.O. Box 12321
Austin Texas

This document is released for the purpose of information exchange review and planning only under the authority of Tony L. Smith, P.E., October 27, 2023, TX PE#92620.

Subject: Hydrologic Variance Request for the Determination of Water Availability and Water Supplies for the 2026 North East Texas Regional Water Plan (Region D)

Dear Mr. Ellis:

The North East Texas Regional Water Planning Group (NETRWPG; Region D) met on October 4, 2023 to discuss the process for determining the amount of surface water available from existing surface water sources and future water management strategies using the guidance provided by the Texas Water Development Board (TWDB) in the scope of work for the present cycle of Regional Water Planning. During this meeting, the NETRWPG discussed the approach for determining water availability within the region, noting where specific variances from the standard TWDB guidance will be employed towards development of the 2026 North East Texas Regional Water Plan.

The NETRWPG approved submittal of this letter and the accompanying attachments, requesting that the TWDB allow the NETRWPG to use the approaches detailed herein throughout the regional planning process for analyses that determine surface water availability to existing rights, availability of groundwater sources, and for analyses to determine the potential supplies available from new water management strategies and water management strategy projects.

Surface Water Supplies

The Region D planning area is located primarily within the Cypress Creek, Red River, Sabine, and Sulphur River Basins. Small areas of the region are in the Neches and Trinity River Basins. Surface waters in each of these river basins serve as a source of water to Region D. In its guidelines for Regional Water Planning, the TWDB requires that water availability be based on results derived from the official Texas Commission on Environmental Quality (TCEQ) Water Availability Models (WAMs), unless a hydrologic variance request is submitted.

The TCEQ WAMs, which have been developed for all river basins in Texas, simulate the management, operation, and use of streamflow and reservoirs over a historical period of record, adhering to the prior appropriation doctrine that governs Texas' water right priority system. The TCEQ WAMs are the fundamental tools used to determine surface water availability for water rights permitting and contain information about water rights in each respective river basin.

There are several versions of each of these WAMs. TWDB guidance stipulates that regional water planning groups use the Full Authorization version that TCEQ employs to analyze applications for perpetual water rights. This scenario is often referred to as WAM "Run 3." The assumptions in the TCEQ WAM Run 3 are conservatively

modeled for permitting purposes, allowing for consideration of water supply availability under drought-of-record conditions to ensure water demands can be met under critical circumstances.

For the purposes of the development of the 2026 Region D Water Plan, the "Run 3" WAMs for each of the aforementioned river basins will be updated to determine surface water availabilities in the region. To reflect the current and future conditions of the region, the following hydrologic variances are summarized below. Hydrologic variance request forms provided by the TWDB have been completed for each river basin, and are included in Attachment A. The methodology for estimating and modeling impacts of sedimentation on the surface water reservoirs are detailed in Attachment B.

Firm Yield

"Firm Yield" is defined in the Texas Administrative Code 31 TAC §357.10 (14) as the:

"maximum amount of water that is physically and legally accessible from existing sources for immediate use by a Water User Group under a repeat of Drought of Record conditions."

In accordance with regional water planning rules and guidance, firm yields for existing reservoirs and water management strategies contemplating a reservoir within Region D will be reported within the 2026 Region D Plan based on the modeled results from the applicable WAM for the basin in which the reservoir is located.

Drought Worse than the Drought of Record

Per TWDB guidance, regional water plans must address water supply needs during a repeat of the drought of record. The generated values of supplies, demands, and population all have associated ranges of uncertainty. Although the limited regional planning resources may not support evaluating a range of or multiple scenarios and although assessments of the likelihood of droughts potentially worse than the drought of record (DWDOR) are not required, RWPGs may choose to consider scenarios and/or qualitatively address uncertainty and DWDOR in their region. Such assessments can be used to more explicitly recognize or acknowledge the relative uncertainties in the planning process and the potential risks without necessarily modifying the plan to mitigate those risks.

If evaluations performed by water providers within Region D include considerations of potential impacts of a DWDOR, these evaluations will be documented within Chapter 8 of the 2026 Region D Plan and considered for informing upon legislative and regional policy recommendations of the NETRWPG within that chapter.

General Hydrologic Assumptions

The NETRWPG will assess surface water availability in a manner that accurately reflects water supplies that are available for use. The NETRWPG requests that the TWDB approve the following assumptions for use in representing existing supplies and potential future surface water supplies in the 2026 Region D Water Plan. The WAMs containing the necessary modifications to the TCEQ WAM that incorporate these assumptions will be referred to as the "Region D WAMs." A general summary of the models and assumptions to be employed for the evaluation of existing water supply and water management strategies (WMS's) is provided below.



Assumption	Use for Existing Supplies	Use for Water Management Strategies
General		
Use most recent available versions of the TCEQ WAMs.	X	X
WAM Run 3 - full consumption of existing water rights with no (zero) return flows).	X	X
Modeling of reuse to include consideration of minimum and permitted return flows associated with WUG, including identified return flows from TCEQ WAM Run 8.	X	X
Channel losses based on factors employed within official TCEQ WAMs.	X	X
ASR evaluations will consider surface water availability as determined by the WAM compared to demand, with the firm supply being the maximum demand that could be met assuming a repetition of the period of record drought.		X
Adopted environmental flow standards will be used as incorporated into the applicable official TCEQ WAMs	X	X
For those basins lacking TCEQ adopted environmental flow standards, TWDB consensus planning criteria will be employed in a manner consistent with TWDB guidelines.		X
Subordination of water rights will be modeled in a manner consistent with modeled subordination within the official TCEQ WAMs.	X	X



Assumption	Use for Existing Supplies	Use for Water Management Strategies
<p>For municipal and industrial users:</p> <p>Run of the river rights will be determined in accordance with TWDB guidelines which state that the use-appropriate monthly percentage of the annual firm diversion must be satisfied in each and every month of the simulation period for all surface water diversions.</p> <p>Reservoirs will use firm yield unless a change is specifically requested by a reservoir owner and approved by the RWPG and TWDB, as appropriate per TWDB guidelines.</p> <p>The calculated source availabilities will be compared against existing legal and infrastructure constraints (water treatment plants, pipelines, intakes, etc.) and will be constrained if the existing infrastructure or legal capability is not sufficient to facilitate full utilization of the source. The most constrained amount will be used as the firm supply.</p>	X	X
<p>For irrigation users, water supply will be determined using firm reliability (100%). In the absence of any supply information or justification of reliable supplies available in a drought of record, supply values will be set equal to zero.</p>	X	X
<p>For livestock, in the absence of any supply information or justification of reliable supplies available in a drought of record, supply values will be set to zero.</p>	X	X



Assumption	Use for Existing Supplies	Use for Water Management Strategies
<i>Sedimentation</i>		
<p>For reservoirs with available volumetric survey information, annual sediment rate will be calculated, and loadings calculated for Year 2030 and Year 2080. Sediment distribution will be calculated using the Empirical Area-Reduction method (more detail on this approach presented in Attachment B) and resultant 2030 and 2080 area-capacity curves developed and employed within WAM. Intervening decadal yields will be linearly interpolated. Evaluations of WMSs will assume original capacities in a conservative manner consistent with TCEQ permitting and TWDB guidelines. This will ensure the use of conservative estimates of availability.</p>	X	X
<p>The most recent volumetric survey information will be utilized. For reservoirs lacking volumetric surveys, original area-capacity relations within TCEQ WAM Run 3 will be assumed constant.</p>	X	X
<i>Groundwater Supplies</i>		
<p>Groundwater availability will be determined using the adopted Modeled Available Groundwater (MAG) numbers. Local hydrogeologic conditions will be considered when establishing each entity's portion of the MAG. For those WUGs/sellers wherein existing or planned pumpage exceeds MAG amounts, amounts derived and adopted for the purposes of the 2021 Region D Plan will formulate the basis for any necessary detailed analysis of the entity's pumping, typical production of the aquifer, and relevant information from applicable GMAs will be considered towards development of the available groundwater supply for the entity. The capability of current infrastructure's (number of wells, well field capacity, peaking factors, etc.) ability to produce annual supply during drought-of-record conditions will also be considered when evaluating future water management strategies. This information will be based upon information</p>	X	X



Assumption	Use for Existing Supplies	Use for Water Management Strategies
developed for the purposes of the 2021 Region D Plan, and similarly coordinated with TWDB subsequent to submittal of the Technical Memorandum.		

Cypress Creek Basin WAM

For the Cypress Creek River Basin, the most recently available official TCEQ WAM Run 3 (ver. June 18, 2015) will be employed for all availability analyses in the basin using the modeled hydrologic period of 1948-1998.

An updated WAM reflecting an extended hydrologic period has been under development by TCEQ and others but has not yet been made publicly available by TCEQ. If the updated official WAM for the Cypress Creek River Basin becomes available prior to the completion of the source water availability modeling task for the purposes of the 2026 Region D Water Plan, the NETRWPG respectfully requests the option to use this updated model for the calculation of water availabilities for existing sources and future strategies within the Cypress Creek River Basin.

Red River Basin WAM

For the Red River Basin, the most recently available official TCEQ WAM Run 3 (ver. Oct. 26, 2021) will be employed for all availability analyses in the basin using the modeled hydrologic period of 1948-2018.

Sabine River Basin WAM

For the Sabine River Basin, the most recently available official TCEQ WAM Run 3 (ver. August 13, 2018) will be employed for all availability analyses in the basin using the modeled hydrologic period of 1940-1998.



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Regarding depictions of sedimentation in Lake Fork and Lake Tawakoni, the area/capacity relations reflecting sedimentation effects will be consistent with those employed by the Region C and Region I RWPGs. This will ensure interregional consistency in reporting. Details on the methodology are described in Attachment B.

Sulphur River Basin WAM

For the Sulphur River Basin, the most recently available official TCEQ WAM Run 3 (ver. Oct. 11, 2019) will be employed for all availability analyses in the basin using the modeled hydrologic period of 1940-2017.

Lake Chapman is currently used by water providers in Region D and Region C and is represented within the official WAM by individual water rights. To assess the firm yield of Lake Chapman, the NETRWPG requests to model the reservoir as a single pool, with supplies then assigned proportionally based on each providers' water rights. This will be done in a coordinated matter with Region C to ensure a consistent representation of the reservoir and supply availability.

The TCEQ WAM Run3 will be modified to correct an error in drainage area for control point C10 (Sulphur River near Talco) as identified by FNI (2012) (see Attachment C):

"In the original TCEQ WAM, primary control point C10, the Sulphur River near Talco (USGS 07343200, aka Sulphur River below Talco 07343210), had a drainage area that was smaller than the next upstream point C20. This results in a flow discontinuity which may impact water availability. Apparently the USGS moved the gage downstream just after the naturalized flows were developed for the Sulphur WAM. For this model, we are using a drainage area for C10 of 1,365 square miles, the drainage area of the gage for the period of the naturalized flows. This is the drainage area used in the original Sulphur WAM."

It has been confirmed that this difference remains in the latest TCEQ Sulphur WAM (October 11, 2019); thus, this correction will be made to all Region D evaluations employing the Sulphur WAM.

Other WAMs

For the purposes of the 2026 Region D Water Plan, for the Neches River Basin the NETRWPG requests use of the Neches WAM model as modified by the Region I RWPG as approved by the TWDB for all availability analyses in the basin. For the Trinity River Basin, the NETRWPG requests use of the Trinity WAM model as modified by the Region C RWPG and approved by the TWDB for all availability analyses in the basin.

Specifics regarding surface water availability modeling of each river basin are presented by basin in the completed hydrologic variance forms provided in Attachment A. Considerations regarding the simulation of reservoir conditions with respect to sedimentation effects are then subsequently detailed in Attachment B. Supporting documentation is provided within Attachment C.



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If you have any questions regarding this request, please contact me at your convenience. We appreciate the TWDB's consideration of this request.

Sincerely,
CAROLLO ENGINEERS, INC.

Tony L. Smith, P.E.
Project Manager

tls

Enclosures: Attachments A, B, C

cc: Jim Thompson
Kyle Dooley
Stan Hayes



Surface Water Hydrologic Variance Request Checklist

Texas Water Development Board (TWDB) rules¹ require that regional water planning groups (RWPG) use most current Water Availability Models (WAM) from the Texas Commission on Environmental Quality (TCEQ) and assume full utilization of existing water rights and no return flows for surface water supply analysis. Additionally, evaluation of existing stored surface water available during Drought of Record conditions must be based on Firm Yield using anticipated sedimentation rates. However, the TWDB rules also allow, and **we encourage**, RWPGs to use more representative, water availability modeling assumptions; better site-specific information; or justified operational procedures other than Firm Yield with written approval (via a Hydrologic Variance) from the Executive Administrator in order to better represent and therefore prepare for expected drought conditions.

RWPGs must use this checklist, which is intended to save time and reduce effort, to request a Hydrologic Variance for estimating the availability of surface water sources. For Questions 4 – 10, please indicate whether the requested variance is for determining Existing Supply, Strategy Supply, or both. Please complete a separate checklist for each river basin in which variances are being requested.

Water Planning Region: D

1. Which major river basin does the request apply to? Please specify if the request only applies part of the basin or only to certain reservoirs.

Cypress Creek Basin

2. Please give a brief, bulleted, description of the requested hydrologic variances including how the alternative availability assumptions vary from rule requirements, how the modifications will affect the associated annual availability volume(s) in the regional water plan, and why the variance is necessary or provides a better basis for planning. You must provide more-detailed descriptions in the subsequent checklist questions. Attach any available documentation supporting the request.

- Request inclusion of return flows for existing surface water rights utilizing return flows for evaluation of existing and strategy reuse supplies. This variance will allow for the evaluation of reuse strategies in the WAM in a manner consistent with present permitting approaches, and thus provides a better basis for planning availabilities of such strategies to WUGs and WWP.

3. Was this request submitted in a previous planning cycle? If yes, please indicate which cycle and note how it is different, if at all, from the previous request?

Yes

¹ 31 Texas Administrative Code (TAC) §§ 357.10(14) and 357.32(c)

The above requests were submitted in the 2021 and 2016 planning cycles and are unchanged from the previous planning cycle request.

4. Are you requesting to extend the period of record beyond the current applicable WAM hydrologic period? If yes, please describe the proposed methodology. Indicate whether you believe there is a new drought of record in the basin.

No

Choose an item.

Click or tap here to enter text.

5. Are you requesting to use a reservoir safe yield? If yes, please describe in detail how the safe yield would be calculated and defined, which reservoir(s) it would apply to, and why the modification is needed or preferable for drought planning purposes.

No

Choose an item.

Click or tap here to enter text.

6. Are you requesting to use a reservoir yield other than firm yield or safe yield? If yes, please describe, in a bulleted list, each modification requested including how the alternative yield was calculated, which reservoir(s) it applies to, and why the modification is needed or preferable for drought planning purposes. Examples of alternative reservoir yield analyses may include using an alternative reservoir level, conditional reliability, or other special reservoir operations.

No

Choose an item.

Click or tap here to enter text.

7. Are you requesting to use a different model (such as a RiverWare or Excel-based models) than RUN 3 of the applicable TCEQ WAM? If yes, please describe the model being considered including how it incorporates water rights and prior appropriation and how it is more conservative than RUN 3 of the applicable TCEQ WAM.

No

Choose an item.

Click or tap here to enter text.

8. Are you requesting to use a modified TCEQ WAM? If yes, please describe in a bulleted list all modifications in detail including all specific changes to the WAM and whether the modified WAM is more conservative than the TCEQ WAM RUN 3. Examples of WAM modifications may include adding subordination agreements, contracts, updated water rights, modified spring flows, updated lake evaporation, updated sedimentation², system or reservoir operations, or special operational procedures into the WAM.

Yes

Existing and Strategy Supply

Updated sedimentation will be represented within the WAM for the determination of reservoir firm yields for existing and strategy supply. A description of the sedimentation methodology to be employed is provided in Attachment B. In the evaluation of a surface water WMS, original reservoir capacities will be used to represent other reservoirs such that the most conservative representation of availability is determined for a WMS (where other reservoirs have full legal access to their storage).

9. Are you requesting to include return flows in the modeling? If yes, are you doing so to model an indirect reuse water management strategy (WMS)? Please provide complete details regarding the proposed methodology for determining reuse WMS availability.

Yes

Existing and Strategy Supply

Evaluations of reuse strategies will use the minimum monthly return flows from the most recent 10-yr historical discharge data of the WUG for which consideration of a reuse water management strategy is evaluated. This approach is consistent with the methods employed by TCEQ in their evaluations of reuse during their permitting process where the permitted, minimum historical, and present discharges relevant to a particular WUG are all considered in the evaluation of a reuse permit.

10. Are any of the requested Hydrologic Variances also planned to be used by another region for the same basin? If yes, please indicate the other Region. Please indicate if unknown.

No

[Click or tap here to enter text.](#)

² Updating anticipated sedimentation rates does not require a hydrologic variance under 31 TAC § 357.10(14). The Technical Memorandum will require providing details regarding the sedimentation methodology utilized. Please consider providing that information with this request.

11. Please describe any other variance requests not captured on this checklist or add any other information regarding the variance requests on this checklist.

Not Applicable

The above requests were submitted in the 2021 and 2016 planning cycles and are unchanged from the previous planning cycle request.

4. Are you requesting to extend the period of record beyond the current applicable WAM hydrologic period? If yes, please describe the proposed methodology. Indicate whether you believe there is a new drought of record in the basin.

No

Choose an item.

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No

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No

Choose an item.

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Yes

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Yes

Existing and Strategy Supply

Evaluations of reuse strategies will use the minimum monthly return flows from the most recent 10-yr historical discharge data of the WUG for which consideration of a reuse water management strategy is evaluated. This approach is consistent with the methods employed by TCEQ in their evaluations of reuse during their permitting process where the permitted, minimum historical, and present discharges relevant to a particular WUG are all considered in the evaluation of a reuse permit.

10. Are any of the requested Hydrologic Variances also planned to be used by another region for the same basin? If yes, please indicate the other Region. Please indicate if unknown.

No

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11. Please describe any other variance requests not captured on this checklist or add any other information regarding the variance requests on this checklist.

Not Applicable.

Surface Water Hydrologic Variance Request Checklist

Texas Water Development Board (TWDB) rules¹ require that regional water planning groups (RWPG) use most current Water Availability Models (WAM) from the Texas Commission on Environmental Quality (TCEQ) and assume full utilization of existing water rights and no return flows for surface water supply analysis. Additionally, evaluation of existing stored surface water available during Drought of Record conditions must be based on Firm Yield using anticipated sedimentation rates. However, the TWDB rules also allow, and **we encourage**, RWPGs to use more representative, water availability modeling assumptions; better site-specific information; or justified operational procedures other than Firm Yield with written approval (via a Hydrologic Variance) from the Executive Administrator in order to better represent and therefore prepare for expected drought conditions.

RWPGs must use this checklist, which is intended to save time and reduce effort, to request a Hydrologic Variance for estimating the availability of surface water sources. For Questions 4 – 10, please indicate whether the requested variance is for determining Existing Supply, Strategy Supply, or both. Please complete a separate checklist for each river basin in which variances are being requested.

Water Planning Region: D

1. Which major river basin does the request apply to? Please specify if the request only applies part of the basin or only to certain reservoirs.

Sabine River Basin

2. Please give a brief, bulleted, description of the requested hydrologic variances including how the alternative availability assumptions vary from rule requirements, how the modifications will affect the associated annual availability volume(s) in the regional water plan, and why the variance is necessary or provides a better basis for planning. You must provide more-detailed descriptions in the subsequent checklist questions. Attach any available documentation supporting the request.

- Request inclusion of return flows for existing surface water rights utilizing return flows for evaluation of existing and strategy reuse supplies. This variance will allow for the evaluation of reuse strategies in the WAM in a manner consistent with present permitting approaches, and thus provides a better basis for planning availabilities of such strategies to WUGs and WWP.

3. Was this request submitted in a previous planning cycle? If yes, please indicate which cycle and note how it is different, if at all, from the previous request?

Yes

¹ 31 Texas Administrative Code (TAC) §§ 357.10(14) and 357.32(c)

The above requests were submitted in the 2021 and 2016 planning cycles and are unchanged from the previous planning cycle request.

4. Are you requesting to extend the period of record beyond the current applicable WAM hydrologic period? If yes, please describe the proposed methodology. Indicate whether you believe there is a new drought of record in the basin.

No

Choose an item.

Click or tap here to enter text.

5. Are you requesting to use a reservoir safe yield? If yes, please describe in detail how the safe yield would be calculated and defined, which reservoir(s) it would apply to, and why the modification is needed or preferable for drought planning purposes.

No

Choose an item.

Click or tap here to enter text.

6. Are you requesting to use a reservoir yield other than firm yield or safe yield? If yes, please describe, in a bulleted list, each modification requested including how the alternative yield was calculated, which reservoir(s) it applies to, and why the modification is needed or preferable for drought planning purposes. Examples of alternative reservoir yield analyses may include using an alternative reservoir level, conditional reliability, or other special reservoir operations.

No

Choose an item.

Click or tap here to enter text.

7. Are you requesting to use a different model (such as a RiverWare or Excel-based models) than RUN 3 of the applicable TCEQ WAM? If yes, please describe the model being considered including how it incorporates water rights and prior appropriation and how it is more conservative than RUN 3 of the applicable TCEQ WAM.

No

Choose an item.

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8. Are you requesting to use a modified TCEQ WAM? If yes, please describe in a bulleted list all modifications in detail including all specific changes to the WAM and whether the modified WAM is more conservative than the TCEQ WAM RUN 3. Examples of WAM modifications may include adding subordination agreements, contracts, updated water rights, modified spring flows, updated lake evaporation, updated sedimentation², system or reservoir operations, or special operational procedures into the WAM.

Yes

Existing and Strategy Supply

Updated sedimentation will be represented within the WAM for the determination of reservoir firm yields for existing and strategy supply. A description of the sedimentation methodology to be employed is provided in Attachment B. In the evaluation of a surface water WMS, original reservoir capacities will be used to represent other reservoirs such that the most conservative representation of availability is determined for a WMS (where other reservoirs have full legal access to their storage).

9. Are you requesting to include return flows in the modeling? If yes, are you doing so to model an indirect reuse water management strategy (WMS)? Please provide complete details regarding the proposed methodology for determining reuse WMS availability.

Yes

Existing and Strategy Supply

Evaluations of reuse strategies will use the minimum monthly return flows from the most recent 10-yr historical discharge data of the WUG for which consideration of a reuse water management strategy is evaluated. This approach is consistent with the methods employed by TCEQ in their evaluations of reuse during their permitting process where the permitted, minimum historical, and present discharges relevant to a particular WUG are all considered in the evaluation of a reuse permit.

10. Are any of the requested Hydrologic Variances also planned to be used by another region for the same basin? If yes, please indicate the other Region. Please indicate if unknown.

Yes

² Updating anticipated sedimentation rates does not require a hydrologic variance under 31 TAC § 357.10(14). The Technical Memorandum will require providing details regarding the sedimentation methodology utilized. Please consider providing that information with this request.

Modeling of the Sabine WAM will be consistent between Region D and Region I. Information from this modeling will also be consistently reported in coordination with Region C.

11. Please describe any other variance requests not captured on this checklist or add any other information regarding the variance requests on this checklist.

Not Applicable

Surface Water Hydrologic Variance Request Checklist

Texas Water Development Board (TWDB) rules¹ require that regional water planning groups (RWPG) use most current Water Availability Models (WAM) from the Texas Commission on Environmental Quality (TCEQ) and assume full utilization of existing water rights and no return flows for surface water supply analysis. Additionally, evaluation of existing stored surface water available during Drought of Record conditions must be based on Firm Yield using anticipated sedimentation rates. However, the TWDB rules also allow, and **we encourage**, RWPGs to use more representative, water availability modeling assumptions; better site-specific information; or justified operational procedures other than Firm Yield with written approval (via a Hydrologic Variance) from the Executive Administrator in order to better represent and therefore prepare for expected drought conditions.

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Water Planning Region: D

1. Which major river basin does the request apply to? Please specify if the request only applies part of the basin or only to certain reservoirs.

Sulphur River Basin

2. Please give a brief, bulleted, description of the requested hydrologic variances including how the alternative availability assumptions vary from rule requirements, how the modifications will affect the associated annual availability volume(s) in the regional water plan, and why the variance is necessary or provides a better basis for planning. You must provide more-detailed descriptions in the subsequent checklist questions. Attach any available documentation supporting the request.
 - Request to correct the TCEQ WAM Run3 for the Sulphur River Basin for the drainage area at Control Point C10. This will increase model accuracy and thus provides an improved basis for planning.
 - Request inclusion of return flows for existing surface water rights utilizing return flows for evaluation of existing and strategy reuse supplies. This variance will allow for the evaluation of reuse strategies in the WAM in a manner consistent with present permitting approaches, and thus provides a better basis for planning availabilities of such strategies to WUGs and WWP.

¹ 31 Texas Administrative Code (TAC) §§ 357.10(14) and 357.32(c)

- Request modeling of Lake Chapman as one pool instead of multiple pools to facilitate calculation of the firm yield. This will increase model accuracy and thus provides an improved basis for planning.

3. Was this request submitted in a previous planning cycle? If yes, please indicate which cycle and note how it is different, if at all, from the previous request?

Yes

The above requests were submitted in the 2021 and 2016 planning cycles and are unchanged from the previous planning cycle request.

4. Are you requesting to extend the period of record beyond the current applicable WAM hydrologic period? If yes, please describe the proposed methodology. Indicate whether you believe there is a new drought of record in the basin.

No

Choose an item.

[Click or tap here to enter text.](#)

5. Are you requesting to use a reservoir safe yield? If yes, please describe in detail how the safe yield would be calculated and defined, which reservoir(s) it would apply to, and why the modification is needed or preferable for drought planning purposes.

No

Choose an item.

[Click or tap here to enter text.](#)

6. Are you requesting to use a reservoir yield other than firm yield or safe yield? If yes, please describe, in a bulleted list, each modification requested including how the alternative yield was calculated, which reservoir(s) it applies to, and why the modification is needed or preferable for drought planning purposes. Examples of alternative reservoir yield analyses may include using an alternative reservoir level, conditional reliability, or other special reservoir operations.

No

Choose an item.

[Click or tap here to enter text.](#)

7. Are you requesting to use a different model (such as a RiverWare or Excel-based models) than RUN 3 of the applicable TCEQ WAM? If yes, please describe the model being considered

including how it incorporates water rights and prior appropriation and how it is more conservative than RUN 3 of the applicable TCEQ WAM.

No

Choose an item.

Click or tap here to enter text.

- 8. Are you requesting to use a modified TCEQ WAM? If yes, please describe in a bulleted list all modifications in detail including all specific changes to the WAM and whether the modified WAM is more conservative than the TCEQ WAM RUN 3. Examples of WAM modifications may include adding subordination agreements, contracts, updated water rights, modified spring flows, updated lake evaporation, updated sedimentation², system or reservoir operations, or special operational procedures into the WAM.

Yes

Existing and Strategy Supply

The TCEQ WAM Run3 will be modified to correct an error in drainage area for control point C10 (Sulphur River near Talco) as identified by FNI (2012) (see Attachment C):

"In the original TCEQ WAM, primary control point C10, the Sulphur River near Talco (USGS 07343200, aka Sulphur River below Talco 07343210), had a drainage area that was smaller than the next upstream point C20. This results in a flow discontinuity which may impact water availability. Apparently the USGS moved the gage downstream just after the naturalized flows were developed for the Sulphur WAM. For this model, we are using a drainage area for C10 of 1,365 square miles, the drainage area of the gage for the period of the naturalized flows. This is the drainage area used in the original Sulphur WAM."

It has been confirmed that this difference remains in the latest TCEQ Sulphur WAM (October 11, 2019); thus, this correction will be made to all Region D evaluations employing the Sulphur WAM. Specifically, the .DIS file will be modified as follows:

** FNI Change - Changed the drainage area for C10 to match USGS drainage area at Sulphur River Near Talco (1,365 mi²) prior to May 21, 1997.

WP	C10	1365	69.6	43.4
**WP	C10	1353.24	69.6	43.4

Lake Chapman is currently used by water providers in Region D and Region C and is represented within the official WAM by individual water rights. To assess the firm yield of Lake Chapman, the NETRWPG requests to model the reservoir as a single pool, with supplies then assigned proportionally based on each providers' water rights. This will be done in a

² Updating anticipated sedimentation rates does not require a hydrologic variance under 31 TAC § 357.10(14). The Technical Memorandum will require providing details regarding the sedimentation methodology utilized. Please consider providing that information with this request.

coordinated matter with Region C to ensure a consistent representation of the reservoir and supply availability.

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Updated sedimentation will be represented within the WAM for the determination of reservoir firm yields for existing and strategy supply. A description of the sedimentation methodology to be employed is provided in Attachment B. In the evaluation of a surface water WMS, original reservoir capacities will be used to represent other reservoirs such that the most conservative representation of availability is determined for a WMS (where other reservoirs have full legal access to their storage).

9. Are you requesting to include return flows in the modeling? If yes, are you doing so to model an indirect reuse water management strategy (WMS)? Please provide complete details regarding the proposed methodology for determining reuse WMS availability.

Yes

Existing and Strategy Supply

Evaluations of reuse strategies will use the minimum monthly return flows from the most recent 10-yr historical discharge data of the WUG for which consideration of a reuse water management strategy is evaluated. This approach is consistent with the methods employed by TCEQ in their evaluations of reuse during their permitting process where the permitted, minimum historical, and present discharges relevant to a particular WUG are all considered in the evaluation of a reuse permit.

10. Are any of the requested Hydrologic Variances also planned to be used by another region for the same basin? If yes, please indicate the other Region. Please indicate if unknown.

No

Click or tap here to enter text.

11. Please describe any other variance requests not captured on this checklist or add any other information regarding the variance requests on this checklist.

Not Applicable.

NORTH EAST TEXAS REGIONAL WATER PLANNING GROUP

2026 Region D Water Plan

Project No.: 200343
Date: October 4, 2023
Prepared By: Michael Pinckney, P.E. and Tony Smith P.E.
Reviewed By:
Subject: Methodology to Estimate Revised Reservoir Storage Volume Capacity and Surface Area Curves for Use in Estimating Existing and Strategy Reservoir Source Availabilities for Future Planning Decades for the purposes of 2026 Texas Regional Water Plan

This document is released for the purpose of information exchange review and planning only under the authority of Tony L. Smith, P.E., 9/21/2023, Texas, PE #92620.

SIMULATION OF RESERVOIR CONDITIONS (SEDIMENTATION)

Reservoir sedimentation reduces the storage capacity of a reservoir, impacting the beneficial uses of reservoirs such as water supply, flood control, hydropower, navigation, and recreation. Surveys of volumetric storage in a reservoir allow for the derivation of rates and loadings of sediment to the reservoir. The annual loading can then be distributed to determine a revised elevation-area-capacity curve which reflects the distribution of the total volume of sediment accumulated at the end of an analysis period. The resultant area-capacity relationship can then be incorporated into an applicable Water Availability Model (WAM) for a given reservoir.

Generally, for the purposes of the 2026 Region D Plan, if a reservoir is calculated to have no firm yield, that result will be assumed for all decades in the 2030-2080 planning horizon. For those reservoirs lacking volumetric surveys, original area-capacity relations employed within WAM Run 3 will be assumed constant. If original area-capacity-elevation relations are not available, the most recent area-capacity-elevation relation for a reservoir will be used as a baseline for future projections. For reservoirs with available volumetric survey information, an annual sediment rate will be calculated or cited from available information, and loadings calculated for Year 2030 and Year 2080. Sediment distribution within the reservoir will be calculated using the Empirical Area Reduction Method (described below), and resultant 2030 and 2080 area-capacity curves will be developed and employed within the applicable WAM to calculate 2030 and 2080 firm yields. The intervening decadal firm yields will then be linearly interpolated.

Empirical Area-Reduction Method

USACE (1989) describes methods for estimating the distribution of sediment deposits in reservoirs. It is noted that empirical methods offer a simple approach useful as a "first approximation," but that their use sacrifices consideration of unique interactions between numerous factors affecting the distribution of

sediment deposits in a given reservoir. Such factors include a reservoir's size, shape, sediment quantities and characteristics, sediment sources, progressive vegetative growth on frequently exposed deposits, consolidation of deposits, basin hydrology, and regulation of the reservoir (USACE, 1989).

While five empirical methods are considered in USACE (1989), two are noted as being the most widely used: the Area-Increment Method and the Empirical Area Reduction Method. For the Area-Increment Method, USACE (1989) notes that, "under extreme reservoir operation conditions, or unusual reservoir shape, the Empirical Area Reduction Method should be used," but also notes that both the Area-Increment method and Empirical Area Reduction method, "tend to overpredict the volume of deposits in the conservation pool."

Such a tendency is considered in the present context as being reasonably conservative, as such an overprediction in the volume of sediment deposits would limit the volume available in the conservation pool. More detailed information and modeling beyond the present scope of the regional planning process would be necessary to provide a more detailed characterization of sediment distribution for individual reservoirs in Region D. Given these considerations, it has been assumed that the Empirical Area Reduction Method is sufficient for the purposes of the 2026 Region D Plan. A brief summary of the Empirical Area Reduction Method to be employed for distribution of sediment is provided below.

The Empirical Area-Reduction Method for calculating the distribution of sediment deposits in a reservoir was developed by Borland and Miller (1958) for the Bureau of Reclamation. The basic equation of the empirical area-reduction method is expressed as

$$S = \int_0^{y_0} A d_y + \int_{y_0}^H K a_p d_y$$

Where,

S = Total sediment volume distributed in the reservoir, typically the volume anticipated to occur in a planning period, e.g. 100-years

o = The original zero elevation of the dam

y_o = The zero elevation of the dam after sediment inflow

A = Reservoir surface area at depth y

d_y = incremental depth

H = Total depth of reservoir commonly determined by the normal water surface

K = a constant of proportionality for converting relative areas to actual areas for a given reservoir

a_p = relative area

p = relative depth

The equation for relative area is expressed as:

$$a_p = Cp^m(1 - p)^n$$

Where, C, m and n are coefficients for four standard reservoir types, summarized in Table 1 as reported by the Sedimentation Section of the Bureau of Reclamation (1962). Values were originally developed by Borland & Miller (1958) and have since been refined by Lara (1962).

Table 1: Reservoir types and values of M, C, m, and n

Reservoir Type	Standard Classification	M	C	m	n
Lake	I	3.5-4.5	5.074	1.85	0.35
Flood Plain Foothill	II	2.5-3.5	2.487	0.57	0.41
Hill	III	1.5-2.5	16.967	1.15	2.32
Gorge	IV	1.0-1.5	1.486	-0.25	1.34

Per Borland and Miller (1958), reservoirs are classified based on a shape factor (M). The shape factor is found by plotting reservoir depth as the ordinate against reservoir capacity as the abscissa, on a log-log plot. The reciprocal of the slope of the line passing through the data points is defined as M. The Sedimentation Section of the Bureau of Reclamation (1962) developed a computational procedure employing the empirical area-reduction methodology.

In the 2016 Region D Plan, the most significant impacts to reservoir storage due to sedimentation were observed in Lake Wright Patman. Given the significance of known sedimentation issues for the lake, specific application of the above approach is demonstrated below in the context of the available information base. The approach described below, where determined to be relevant in Region D reservoirs, will be employed for those reservoirs where consideration of significant sedimentation effects is warranted.

Lake Wright Patman

Lake Wright Patman (originally known as Lake Texarkana) was authorized in 1946 as a part of a comprehensive plan for flood control in the Red River Basin (TWDB 2003). The deliberate impoundment of Lake Wright Patman began June 27, 1956, the reservoir water level reached conservation pool elevation in February 1957. The reported original volumetric capacity of the reservoir is 158,000 ac-ft (TWDB, 2010). Two volumetric surveys of the reservoir have been performed by TWDB over the last several decades, described below:

1997 Hydrographic Survey

The Texas Water Development Board conducted a hydrographic survey of Wright Patman Lake during the period December 16 – January 16, 1997 to determine the capacity of the lake at the conservation pool and when the lake was in the flood pool (TWDB 2003). The results of this TWDB survey indicate that the lake’s capacity at the conservation pool elevation of 220.6 ft. mean sea level (msl) was 110,900 acre-feet and the area was 18,994 acres. At elevation 230 ft. (msl) the volume was determined to be 392,740 acre-feet with an area of 34,882 acres (TWDB 2003). The estimated reduction in storage capacity at elevation 220.6 ft. (msl) since 1956 was 34,400 acre-ft or 1,147 acre-ft per year. At elevation 230 ft. (msl), the reduction in storage calculated was 44,510 acre-feet or 1,483.7 acre-feet per year (TWDB 2003).

2010 Hydrographic Survey

The Texas Water Development Board conducted a hydrographic survey of Lake Wright Patman during the period between March 26 – June 7, 2010 to determine the volumetric capacity of the

lake. The results of the TWDB's 2010 survey indicate that the lake's 2010 capacity at the conservation pool elevation of 220.6 ft. (msl) was 97,927 acre-feet, with an area of 18,247 acres. Additionally, refinements in the methodology for calculating reservoir capacity from collected bathymetry prompted the TWDB to re-analyze the 1997 volumetric survey data (TWDB 2010). This re-analysis of the 1997 TWDB volumetric survey resulted in an updated 1997 capacity estimate at 220.6 ft. (msl) of 115,715 acre-feet using the 1997 survey data.

TWDB then calculated sediment rates at 220.6 ft (msl) for three scenarios:

1. The difference between the 2010 surveyed capacity and the original design capacity estimate;
2. The difference between the 2010 surveyed capacity and an estimation of the pre-impoundment capacity performed in 2010; and
3. The difference between the 2010 surveyed capacity and the revised 1997 surveyed capacity estimate.

These calculations and supporting data are presented in Table 2.

Table 2 - Capacity loss comparisons for Lake Wright Patman (recreated from TWDB 2010)

Survey	Comparisons @ 220.6		
	Volume (acre-ft)		Pre-impoundment (acre-ft)
	Comparison #1	Comparison #2	Comparison #3
Original design estimate ^a	158,000	<>	<>
TWDB pre-impoundment estimate based on 2010 survey	<>	<>	137,336 ^b
1997 TWDB volumetric survey (revised)	<>	115,638	<>
2010 volumetric survey	97,927	97,927	97,927
Volume difference (acre-ft)	60,073 (38%)	17,711 (15.3%)	39,409 (28.7%)
Number of years	54	13	54
Capacity loss rate (acre-ft/year)	1,112	1,362	730

^a Source: (TWDB, 1974), note: Wright Patman Dam was completed on May 19, 1954, and deliberate impoundment began on June 27, 1956.

^b 2010 TWDB surveyed capacity of 97,927 acre-feet plus 2010 TWDB surveyed sediment volume of 39,409 acre-feet.

In July 2018, Riverbend Water Resources District contracted a volumetric and sedimentation survey of Lake Wright Patman, which was conducted between July 17, 2018 and August 23, 2018 by Arroyo Environmental Consultants, LLC and partner firm Aqua Strategies Inc. The results of Arroyo's survey indicate that the lake's capacity at the conservation pool elevation of 220.6 ft. (msl) was 96,430 acre-feet

and the area was 17,907 acres. At elevation 224 ft. (msl) the volume was determined to be 168,736 acre-feet with an area of 24,343 acres (Arroyo 2019).

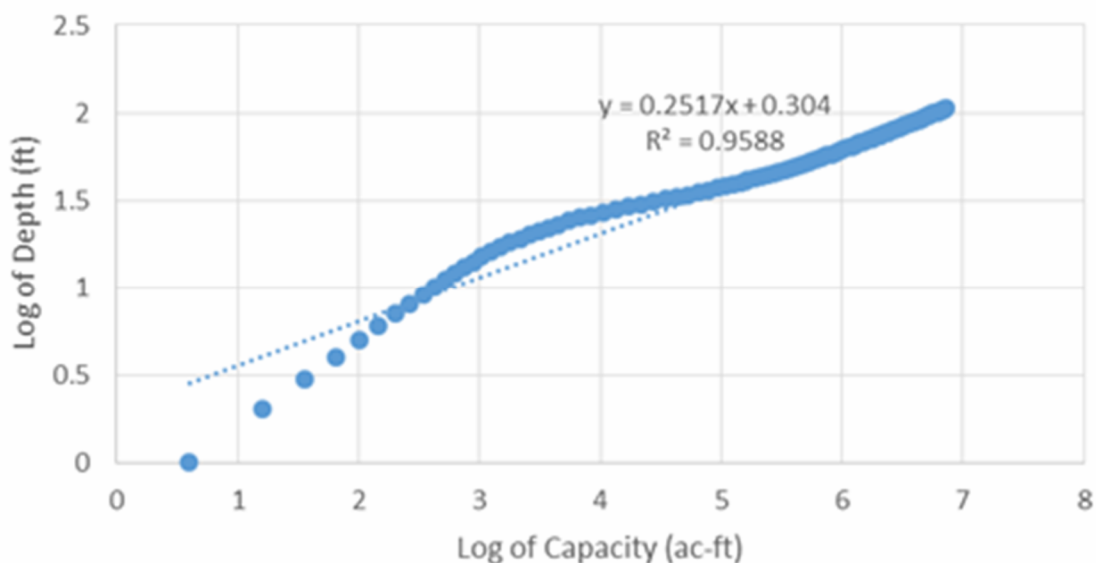
Based on the data collected in the survey, Arroyo estimated the pre-impoundment volume to be 126,752 ac-ft at elevation 220.6 ft. (msl) and 205,121 ac-ft at elevation 224 ft. (msl). The estimated reduction in storage capacity at elevation 220.6 ft. (msl) since 1956, based on the estimated pre-impoundment volume, was 30,322 acre-ft or 489 acre-ft per year. At elevation 224 ft. (msl), the reduction in storage calculated was 36,385 acre-ft or 587 acre-ft per year. Relative to the original design volume estimates, at elevation 220.6 ft. (msl) there is an estimated capacity loss of 61,570 ac-ft and at elevation 224.0 ft. (msl) a capacity loss of 71,459 ac-ft (Arroyo 2019).

Arroyo (2019) estimates annual losses in Lake Wright Patman's capacity ranges between 187 and 993 acre-feet (based on the original, re-analyzed 1997, and 2010 capacities, respectively) at 220.6 ft (msl) due to sedimentation below the conservation pool elevation. Given that Lake Wright Patman is a flood control reservoir, it is thus necessary to derive an overall sedimentation rate for the entire reservoir (i.e., from bottom elevation up to the top of dam elevation) to develop overall area-capacity relations.

To develop the overall sedimentation rate for use in projecting future reservoir sedimentation, the rate of capacity loss due to sedimentation at 220.6 ft (msl) has been assumed as 714 ac-ft/yr, as this loss rate derives from an average of the comparison of the Arroyo 2018 surveyed capacity of 96,430 ac-ft compared to the original estimated design capacity of 158,000 ac-ft, 2010 estimated pre-impoundment volume of 137,366 ac-ft, and the 2018 estimated pre-impoundment volume of 126,752 ac-ft. This estimated rate is not as aggressive a loss rate as the 1,362 ac-ft/yr rate derived from comparing the 2010 to the 1997 TWDB surveys, but represents the longer term effects of sediment deposition in the reservoir at 220.6 ft. (msl).

Using the original design elevation-area-capacity relationship as a basis, the shape factor (M) is calculated using the previously described log-log plot of reservoir depth vs. capacity (Borland and Miller, 1958), as shown in Figure 1 for Lake Wright Patman.

Figure 1 - Log-Log Plot of Reservoir Depth vs. Capacity with Best Fit Regression for Lake Wright Patman



The resultant shape factor is the reciprocal of the slope of the best fit regression (i.e. $M = 1/.2517 = 3.97$). The standards classification for this shape factor for Lake Wright Patman is a "Type I" reservoir. Thus, the equation for the calculation of relative area to be used in the Empirical Area Reduction Method for Lake Wright Patman is as follows:

$$a_p = 5.074p^{1.85}(1 - p)^{0.35} \quad (\text{Eq. 1})$$

With an equation for relative area and the original design relationship between elevation, area, and capacity for the reservoir, a calculated sedimentation volume at a known elevation to be distributed from the original design capacity curve to the surveyed capacity curve, and a sedimentation rate for future sedimentation, area-capacity relationships at future decadal times over the planning horizon (2030 - 2080) can be developed.

Per the Riverbend Water Resource District's request during the development of the 2021 RWP, the new Elevation Area Capacity data developed by Arroyo in 2018-2019 and given the operating characteristics of the conservation pool of Wright Patman, a pair of sedimentation rates were identified for planning use. The first sedimentation rate of 714 ac-ft/yr is applied to all elevations equal to or below 220.6 ft. (msl) and a sedimentation rate of 824 ac-ft per year is utilized for elevations below 224.9 ft. (msl). Given that the use of K is for modeling the area of sedimentation, more than one K value could be used in the EARM wherein a K value applies at specific elevation ranges. Thus, a single application of the EARM can be derived that meets the observed sedimentation volumes at elevations 220.6 ft. (msl) and 224.9 ft. (msl).

Thus, using the reported sedimentation volume between 1956 and 2018, the original design area capacity curve is adjusted to reflect the distribution of the sediment present in 2018. Using the assumed rate of capacity loss in Lake Wright Patman of 714 ac-ft/yr at elevation 220.6 ft. (msl) and 824 ac-ft/yr at elevation 224.9 ft (msl) for 2018 through the planning decades and the Empirical Area Reduction Method results in new elevation-area-capacity relations for 2030 - 2080 (see Figures 2 and 3). These decadal relations of reservoir area and capacity are then incorporated as inputs to the Sulphur WAM.

Figure 2 - Decadal Relations of Volume to Water Surface Elevation for Lake Wright Patman from Application of Empirical Area Reduction Method for Distribution of Sediment Deposits using Annual Capacity Loss Rate of 714 ac-ft/yr for elevation 220.6 ft. (msl) and below and 824 ac-ft/yr for elevations above 220.6 ft. (msl).

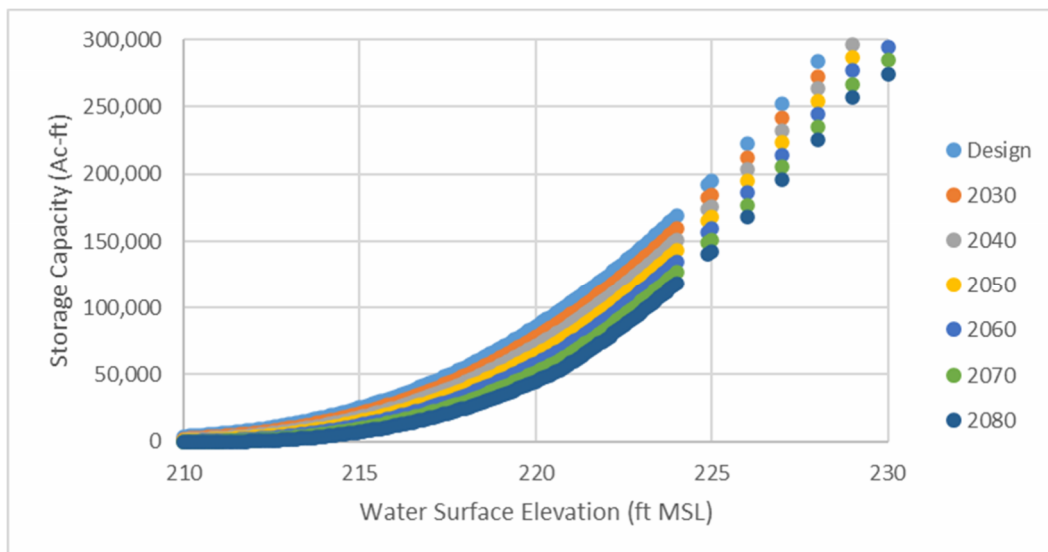
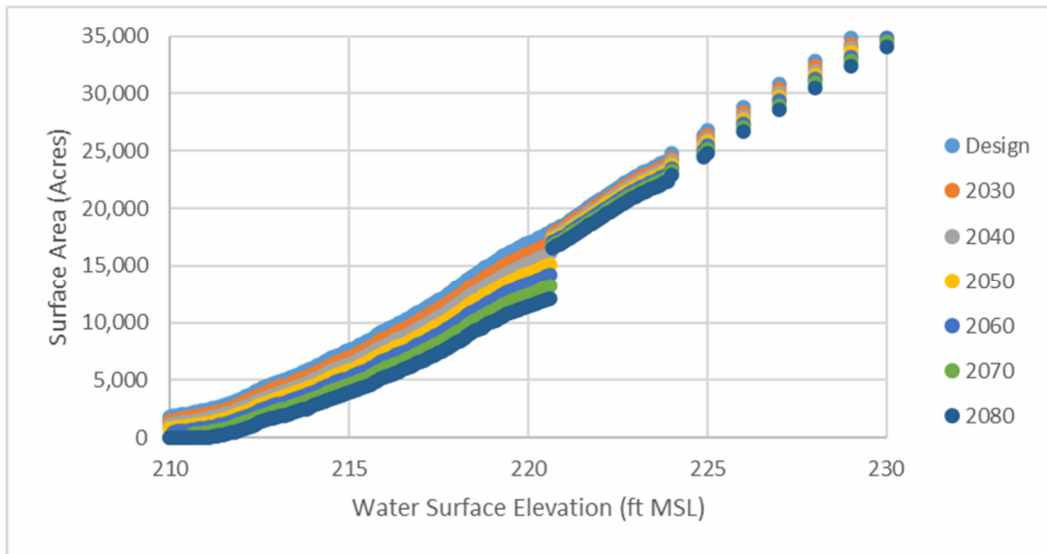


Figure 3: Decadal Relations of Area to Water Surface Elevation for Lake Wright Patman from Application of Empirical Area Reduction Method for Distribution of Sediment Deposits using Annual Capacity Loss Rate of 714 ac-ft/yr for elevation 220.6 ft. (msl) and below and 824 ac-ft/yr for elevations above 220.6 ft. (msl).



Lake Fork and Lake Tawakoni

In coordination with Region C and Region I, the area/capacity relations to be utilized within the WAM reflecting the effects of sedimentation will be the same. The latest volumetric survey information will be utilized to determine sedimentation rates, then the trapezoidal and conical methods for sediment distribution will be used to determine the area/capacity relation for each method. These will be compared to the observed area/capacity relation, and the root mean squared error (RMSE) calculated for each approach. The area/capacity relation resulting from the approach with the least RMSE will then be adopted.

References

- Arroyo Environmental Consultants (2019). Volumetric And Sedimentation Study on Wright Patman Lake, prepared for Riverbend Water Resources District.
- Borland, W.M., & Miller, C.R.(1960). Distribution of sediment in large reservoirs. Transactions, American Society of Civil Engineers, v. 125, p. 166-180.
- Cristofano, E.A. (1953). Area increment method for distributing sediment in a reservoir. U.S. Bureau of Reclamation. Albuquerque, N.M.
- Lara, J.M., (1962). "Revision of the Procedure to Compute Sediment Distribution in Large Reservoirs," US Bureau of Reclamation, Denver, CO.
- TWDB (Texas Water Development Board), 2003. Volumetric Survey of Wright Patman Lake, prepared for U.S. Army Corps of Engineers, Fort Worth District. Austin, TX.
- TWDB (Texas Water Development Board), 2010. Volumetric and Sedimentation Survey of Wright Patman Lake, March - June 2010 Survey, prepared for U.S. Army Corps of Engineers, Fort Worth District, in cooperation with the City of Texarkana. Austin, TX.
- USACE (U.S. Army Corps of Engineers), December 15, 1989, changed October 1995. Engineering and Design - Sedimentation Investigations of Rivers and Reservoirs. EM 1110-2-4000, Appendix H, Washington, DC.

TO: File

CC: Becky Griffith, Tony Smith (Espey)

FROM: Jon Albright and Jeremy Rice

SUBJECT: Modifications to the Sulphur WAM and Preliminary Yields

DATE: July 16, 2012

PROJECT: MHP11453

Freese and Nichols Inc. (FNI) has developed an updated version of the Sulphur Water Availability Model (WAM). This model will be used as the basis for all WAM modeling in the Sulphur Basin Watershed Overview Project. These modifications are primarily based on the Texas Water Development Board's Site Protection Study. The following changes were made to the Sulphur WAM:

- Use of current Storage-Area relationships for Lakes Wright Patman and Jim Chapman
- Use of one pool to model Lake Jim Chapman (this facilitates analyzing the impact of changes on the performance of the reservoir).
- Addition of Lake Ralph Hall based on code from TCEQ.
- Addition of Marvin Nichols Site 1a, Parkhouse I, Parkhouse II and Talco sites.
- Manual input of naturalized flows at the Marvin Nichols and Parkhouse I and II sites to correct for problems with drainage areas in the original Sulphur WAM.
- Changes to correct errors in drainage area for control point C10 (Sulphur River near Talco)

Each of these changes is discussed in more detail below.

Preliminary Reservoir Yields

We have used this model to calculate preliminary firm yields of Marvin Nichols 1a and Parkhouse I and II assuming current sediment conditions, with Lake Ralph Hall in place (see Table 1). Note that these yields are slightly different than the Site Protection Study. There are several reasons for this. First, we are assuming current sediment conditions at Lake Wright Patman and Lake Chapman, where the Site Protection Study used original sediment conditions (Run 3). Second, we are assuming overdraft operation of Lake Ralph Hall without environmental bypass, while the Site Protection Study assumed firm yield operation of Ralph Hall with

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Consensus Bypass. Third, the Site Protection Study yields in Table 1 are the yields without environmental bypass from the Site Protection Study with the estimated impact of Lake Ralph Hall subtracted from the yield. Since the operation of Lake Ralph Hall is different in the Site Protection Study than in the current study, the impact on yield may be a little different. Finally, the Site Protection Study had the flow discontinuity at control point C10, which may have slightly impacted yields.

Table 1: Preliminary Firm Yields

Proposed Reservoir	Calculated Firm Yield (acre-feet per year)	Site Protection Study Firm Yield (acre-feet per year)	Difference (acre-feet per year)
Marvin Nichols 1a	595,000	596,900	-1,900
Parkhouse I	124,600	124,400	200
Parkhouse II	121,800	119,900	1,900

Future yields calculated for the Sulphur Watershed Overview will assume different sediment conditions for Patman, Chapman and Ralph Hall. However, specific sediment scenarios have not been identified at this time.

Yields of the Talco site will be developed at a later date.

Modifications to Sulphur WAM

Lake Chapman

In the TCEQ WAM, Lake Chapman is modeled with three individual pools, reflecting the three water rights in the reservoir. For this study Lake Chapman is modeled as a single pool. This change facilitates analyzing impacts of other projects on the overall performance of Lake Chapman. The instream flow requirements and diversion were also combined into a single IF and WR record. The model for this study uses the 2007 TWDB Volumetric Survey of Lake Chapman rather than the original storage and area characteristics in the TCEQ WAM.

Changes to DAT File

Change instream flow so that it comes from one pool instead of being divided among 3 pools. This release is continuous and not limited to inflow as in the TCEQ code.

```
**IF   A40   951       19651119   3           IF4797
**WSRCHAP1  81470                               1
**IF   A40   2285       19651119   3           IF4798
```

DRAFT Modifications to Sulphur WAM and Preliminary Yields



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```
**WSRCHAP2 114265 1 -1
**IF A40 3619 19651119 3 IF4799
**WSRCHAP3 114265 1 -1
```

**
**

** FNI change: since we are using one pool, we need to change to one IF (5 cfs)

```
**
IF A40 3619 19651119 3 IF_Chapman
WSRCHAP1 298930
OR A40 -1
```

Change from three pools (corresponding to the three water rights in the lake) to a single pool. Redistribute amounts among the various users reflecting current conditions. EA, EF and AF records no longer needed so they are commented out.

```
**WR A40 38520 4797M19651119 1 4797AM_1 A 4797
**WSRCHAP1 81470 1
**
** North Texas Municipal Water District
**WR A40 54000 479819651119 4798_1 A 4798
**WSRCHAP2 114265 1 -1
** City of Irving
**WR A40 54000 4799M19651119 4799M_1 A 4799
**WSRCHAP3 114265 1 -1
```

**

** Upper Trinity Regional Water District

```
WR A40 16106 4797M19651119 1 4797M_UTRWD Chapman 4797
WSRCHAP1 298930 38598
```

**

** Local demand (Sulphur Spr and Cooper)

```
WR A40 19200 4797M19651119 1 4797M_SSPRS Chapman 4797
WSRCHAP1 298930 38598
```



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**

** North Texas Municipal Water District

WR	A40	3214	479819651119		4797_NTMWD Chapman	4797
WSRCHAP1	298930			38598		

**

WR	A40	54000	479819651119		4798_1 Chapman	4798
WSRCHAP1	298930			38598		

**

** City of Irving

WR	A40	54000	4799M19651119		4799M_1 Chapman	4799
WSRCHAP1	298930			38598		

**WSRCHAP1 304101 31101

**

** Original TCEQ WAM. Since we are using one pool we do not need

**EA	1	3	RCHAP1	RCHAP2	RCHAP3
**EF	0	0	.26	.37	
**AF	0	0	.26	.60	1

**

Storage and area relationships from 2007 TWDB survey.

**SVRCHAP1	0	2000	8000	20000	45000	63000	85000	132000	194000	239000	255000	310000
**SA	0	850	1925	2920	5625	6525	8100	10800	13800	16400	17200	19305

**

**FNI Change Based on 2007 Volumetric Survey

**ELEV (ft)	396	402	408	414	420	424	428	432	436	438	439	440
SVRCHAP1	0	901	10189	31426	64164	92257	128478	175115	232754	264866	281565	298930
SA	0	746	2471	4549	6349	7851	10412	12908	15668	16457	16976	17958

**

Lake Wright Patman

Lake Wright Patman is operated by the Corps of Engineers. The Corps uses seasonally varying conservation storage, defined by a rule curve. There are two rule curves for the reservoir:

- Interim Curve – the curve used for current operation of the reservoir.



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- Ultimate Curve – the curve in the Texas Water Right (and the WAM) and certain contracts with the Corps.

Note that there are no downstream releases in the setup. At this time we are planning to include any downstream releases in the yield of the reservoir. This model also uses current area and storage relationships from the draft 2010 volumetric survey.

Changes to DAT File

** FNI Change: Update storage numbers for Patman: 2010 Survey, 297505 af is capacity at 228.6 ft, 87300 af is capacity at 220 ft

** FNI Change - add group identified for Patman

**

WR F60 14572 4836M19510305 4836M1 PATMAN 4836

** Interim Curve - Texarkana Contract Minimum (220 ft)

**WSPATMAN 262808 87300 98162

**

** Ultimate Curve - Texarkana Contract Minimum (220 ft)

WSPATMAN 298084 87300 200411

**

WR F60 10428 4836M19570217 4836M2 PATMAN 4836

WSPATMAN 298084 87300

**

WR F60 20000 4836M19670919 4836M3 PATMAN 4836

** WR 4836I - maximize out of basin transfers for full paper right runs (1,2,3,4,6), transfers deducted from most junior WR fo

WSPATMAN 298084 87300

**

WR F60 35000 4836I19570217 4836I1 PATMAN 4836

WSPATMAN 298084 87300

**

WR F60 100000 4836I19670919 4836I2 PATMAN 4836

WSPATMAN 298084 87300

The Sulphur WAM was also modified to use the Draft 2010 TWDB Volumetric Survey of Lake Wright Patman.

This survey was extended to higher elevations using previous surveys

**SVPATMAN 0 6670 64795 108195 166445 213845 240195 268445 298495 330345 364095 399695

**SA 0 1350 12100 16900 22000 25400 27300 29200 30900 32800 34700 36500



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** FNI change: update SVSA to 2010 survey

**Elev	194	214	219	222	224	226	230	235	241	248	255	260
SVPATMAN	0	18531	70925	125611	171069	220465	340658	542648	858115	1338792	1950548	2473806
SA	0	6243	15397	21231	23924	25435	34882	45924	59567	77777	97430	111880

Interim and Ultimate curves using 2010 survey

** Monthly Storage Variable Limits

**

** Wright Patman

**

** FNI change - based on Interim Rule Curve and 2010 survey

**Month	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
**Elev	220.60	220.60	220.60	224.90	227.44	226.92	226.29	225.67	225.06	220.60	220.60	220.60
**MSPATMAN	98162	98162	98162	192965	262808	246994	227884	212193	196902	98162	98162	98162

** FNI change - based on Ultimate Rule Curve and 2010 survey

**Month	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
**Elev	224.90	224.90	224.90	226.80	228.60	228.60	228.50	227.80	226.80	226.10	225.50	225.20
MSPATMAN	192965	192965	192965	243345	298084	298084	295043	273755	243345	223023	207932	200411

Ralph Hall

TCEQ provided a version of the DAT file for the Sulphur WAM with Lake Ralph on October 6, 2011. This code is for overdraft operation of the reservoir. Typical instream flow bypass criteria are not proposed for this reservoir. The following changes were made to the FNI Sulphur WAM.

Changes to DAT file

** FNI Change - Added used pattern for Ralph Hall

UC HALL	0.0730	0.0650	0.0590	0.0850	0.0690	0.0880
UC	0.1230	0.1470	0.1130	0.0870	0.0520	0.0390

** FNI Change - Added in Ralph Hall

CP158211	B10		7	A70	0
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** FNI Change - Added Ralph Hall

WR158211	45000	HALL20040813	1						15821F	15821F
WS158211	180000									

**

** FNI Change - Added Ralph Hall

** ELEVATION	460	470	480	490	500	510	520	530	540	550	560	564
SV158211	0	57	397	1027	2357	7521	21849	47989	90104	152630	238693	280506
SA	0	17.9	49.6	79.1	208	941	2003	3307	5189	7345	9914	10985

**

Changes to DIS file

TCEQ did not provide a copy of the DIS file. Thus the drainage area was taken from the 2007 TWDB Reservoir Site Protection Study. Memos from TCEQ associated with the draft permit give the drainage area as 102.74 square miles.

** FNI change - Added lake Ralph Hall

FD158211	B10	0
----------	-----	---

** Drainage area based on 2007 Reservoir Site Protection Study

WP158211	101
----------	-----

Marvin Nichols 1a, Parkhouse I and Parkhouse II

Code for Marvin Nichols 1a and Parkhouse I and II are from the Reservoir Site Protection Study. The Site Protection Study model used manually calculated naturalized flows for each of these projects rather than using the model to calculate the flows. The drainage areas in the Sulphur WAM do not match USGS drainage areas. In our opinion, USGS drainage areas are more likely to be accurate. The manually calculated flows are based on the USGS drainage areas. These flows were input at new primary control points. The new flows are included with the setup files that accompany this memo.

The Reservoir Site Protection Study model also included evaporation rates for the new projects. Unlike other evaporation data in the Sulphur WAM, these evaporation rates include corrections for effective runoff based on the naturalized flow at the new primary control points. WRAP does not allow evaporation adjustments at primary control points. The new evaporation files are included with the setup files that accompany this memo.

Changes to DAT file



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** FNI Change - Municipal Use for Marvin Nichols and Parkhouse (I and II) from Site Protection Study
 UC MUN 0.0651 0.0607 0.0648 0.0697 0.0802 0.0951
 UC 0.1161 0.1176 0.1034 0.0905 0.0715 0.0653
 **

** FNI Change - Parkhouse South (I) new primary control point C200
 ** additional control points A,B and C for application of instream flows
 **CP A10 C60 1 D120 -3 0
 CP A10 C200 1 D120 -3 0
 CP C200 C200A 1 -3
 CP C200A C200B 2 C200 NONE
 CP C200B C200C 2 C200 NONE
 CP C200C C60 2 C200 NONE
 **CP C110 C60 7 D120 0
 CP C110 C200 7 D120 0

** FNI Change - Parkhouse North (II) new primary control point C105
 ** additional control points A,B and C for application of instream flows
 ** CP B10 C90 1 D120 -3 0
 **
 CP B10 C105 1 A70 -3 0
 CP C105 C105A 1 -3 0
 CP C105A C105B 2 C105 NONE -3 0
 CP C105B C90 2 C105 NONE -3 0
 **

** FNI Change - Marvin Nichols new primary control point E175
 ** additional control points A,B for application of instream flows
 **CP E250 E10 7 E60 0
 **CP E240 E10 7 E60 0
 CP E250 E175 7 E60 0
 CP E240 E175 7 E60 0
 CP E175 E175A 1 -3 0
 CP E175A E175B 2 E175 NONE -3 0
 CP E175B E10 2 E175 NONE -3 0
 **

** FNI change - CPs E190, E200, E210, and E220 used to flow into E180, which has been eliminated.
 ** change to flow into Marvin Nichols
 **CP E220 E10 7 E60 0
 **CP E210 E10 7 E60 0
 **CP E200 E10 7 E60 0
 **CP E190 E10 7 E60 0
 CP E220 E175 7 E60 0
 CP E210 E175 7 E60 0
 CP E200 E175 7 E60 0
 CP E190 E175 7 E60 0
 **CP D120 D40 7 0



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```
**CP D110 D40 7 D120 0
**CP D100 D40 7 D120 0
```

** PROPOSED PROJECTS FOR STUDY

**

** FNI Change added Parkhouse I

```
WR C200 143600 MUN30000105 PARKHOUSE I
WSPARK I 651712
```

**

** FNI Change added Parkhouse II

```
WR C105 148700 MUN30000105 1 0 0 PARKHOUSE II
WSPARKII 330871
```

**

** FNI Change - added Marvin Nichols

```
WR E175 600900 MUN30000105 1 0 0 MARVIN_NICHOLS
WSMARVIN 1562669 0
```

**

** FNI Change - Marvin Nichols

** Area-Capacity Relationship from Site Protection Study:

```
SVMARVIN 0 23155 42283 101593 229008 483319 614963 765728 1087776 1309166 1562669 1701463
SA 0 5381 7480 12295 20072 30778 35047 40681 51337 59365 67392 71406
```

** FNI Change - Parkhouse I from Site Protection Study

```
SVPARK I 0 12600 49057 121267 204814 265446 357065 466684 567951 680825 802444 932332
SA 0 2925 6168 10120 13752 16566 20084 23808 26828 29372 31439 33506
```

** FNI Change - Parkhouse II from Site Protection Study

```
SVPARKII 0 595 2113 7440 17983 34004 55512 83780 144687 215361 263249 330871
SA 0 111 226 1556 2660 3750 4916 6392 8919 11282 12662 14387
```

**

Changes to DIS file

** FNI Change - New control point for Parkhouse I:

```
WP C200 655.0
```

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WP C200A	655.0		
FD C200A	C200	-1	
WP C200B	655.0		
FD C200B	C200	-1	
WP C200C	655.0		
FD C200C	C200	-1	

**

** FNI Change - New Control Point for Parkhouse II

**

WP C105	421.0		
WP C105A	421.0		
FD C105A	C105	-1	
WP C105B	421.0		
FD C105B	C105	-1	

**

** FNI Change - New control point for Marvin Nichols

WP E175	1889.0		
WP E175A	1889.0		
FD E175A	E175	-1	
WP E175B	1889.0		
FD E175B	E175	-1	

Talco Site

At this time the setup for the Talco site is under development. The project will be at control point C10, which is a primary control point.

Correction to Drainage Areas

In the original TCEQ WAM, primary control point C10, the Sulphur River near Talco (USGS 07343200, aka Sulphur River below Talco 07343210), had a drainage area that was smaller than the next upstream point C20. This results in a flow discontinuity which may impact water availability. Apparently the USGS moved the gage downstream just after the naturalized flows were developed for the Sulphur WAM. For this model, we are

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using a drainage area for C10 of 1365 square miles, the drainage area of the gage for the period of the naturalized flows. This is the drainage area used in the original Sulphur WAM.

Changes to DIS file

** FNI Change - Changed the drainage area for C10 to match USGS drainage area at Sulphur River Near Talco (1,365 mi²) prior to May 21, 1997.

WP C10 1365 69.6 43.4

**WP C10 1353.24 69.6 43.4

**