VOLUMETRIC SURVEY OF BELTON LAKE

Prepared for:

BRAZOS RIVER AUTHORITY



Prepared by:

The Texas Water Development Board

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BELTON LAKE HYDROGRAPHIC SURVEY REPORT

INTRODUCTION

Staff of the Hydrographic Survey Unit of the Texas Water Development Board (TWDB) conducted a hydrographic survey on Belton Lake in September, 1994. The purpose of the survey was to determine the capacity of the lake at the normal pool elevation and to establish baseline information for future surveys. From this information, future surveys will be able to determine sediment deposition locations and rates over time. Survey results are presented in the following pages in both graphical and tabular form. All elevations presented in this report will be reported in feet above mean sea level based on the National Geodetic Vertical Datum of 1929 (NGVD '29) unless noted otherwise. The results will be compared to the information from the latest sedimentation survey performed by the U. S. Army Corps of Engineers in 1966. At the normal pool elevation of 594.0 feet, they reported a surface area of 12,423 acres and a capacity of 441,984 acre-feet.

HISTORY AND GENERAL INFORMATION OF THE RESERVOIR

Belton Lake is located on the Leon River in Bell County, three miles north of Belton, Texas. The estimated drainage area of the lake is 3,531 square miles and includes Cowhouse, Owl, Cedar, and Stampede Creeks. The lake and dam facility are owned by the United States Government, and maintained and operated by the U. S. Army Corps of Engineers, Fort Worth District (COE). The water rights are allocated to the U. S. Government and the Brazos River Authority. Dam construction commenced in July 1949. Deliberate impoundment of water began March 8, 1954 and the facility was completed December 15 of the same year. The project was designed by the COE and the general contractor was J. W. Moorman and Son of Snyder, Texas. The estimated project cost was \$13,804,000.

Belton Dam consists of a rolled-earthfill embankment, 5,524 feet long, with a 1,300 foot uncontrolled broad-crested spillway. The controlled outlet works consists of a 22-foot-diameter conduit that is controlled by three 7-by-22-foot broome-type gates. The service outlet consists of a 36-by-36-inch gated outlet that discharges into the controlled outlet conduit.

Belton Lake was authorized to be built under the Federal Flood Control Act of July 24, 1946, modified on September 3, 1954. Water Rights were granted by the State Board of Water Engineers under Permit No. 1689, dated October 29, 1953, to the U. S. Government to divert 10,000 acre-feet of water per year for use at Fort Hood. This volume of water was later increased to 12,000 acre-feet per year by Permit No.1725 dated October 27, 1954. A Certificate of Adjudication No. 2936 for the same amount of water was issued by the Texas Water Commission on April 30, 1984 to the COE.

Additional water rights from Belton Lake were granted to the Brazos River Authority (BRA) under Permit No. 2108, July 24, 1964. The permit authorized the permittee to impound not to exceed 457,600 acre-feet of water in Belton Lake. BRA could divert and use not to exceed 95,000 acre-feet of water per annum for municipal purposes, 150,000 acre-feet of water per annum for industrial purposes and 150,000 acre-feet per annum for irrigation purposes with a priority right of 110,000 acre-feet of water per annum. Permit No. 2108 was amended by the Texas Water Commission on September 4, 1979. It expanded the rights of the BRA at Belton Lake to include the use of impounded waters for non-consumptive recreational purposes. The permit was further amended on November 30, 1980. It authorized the BRA to use 500 acre-feet for mining purposes out of the 150,000 acre-feet of water allotted for irrigation. Certificate of Adjudication No. 5160 was issued to the BRA on December 14, 1987. It stated the BRA had entered into a contractual agreement with the United States Government for the storage of 457,600 acre-feet of water in Belton Lake between elevation 540 and elevation 594 under the same conditions as previously stated in the amended Permit No. 2108.

The BRA has additional authority to use waters from the Brazos River Basin system. Certificate of Adjudication No. 5167 (issued December 14, 1987) allows the BRA to divert and use not to exceed 30,000 acre-feet of water for municipal purposes and 170,000 acre-feet for industrial purposes in the San Jacinto-Brazos Coastal Basin. These waters are to be released from Belton Lake and other reservoirs owned and operated by the Brazos River Authority.

Belton Lake, at the normal pool elevation of 594.0 feet, was originally estimated when built by the COE to have a capacity of 457,600 acre-feet with a surface area of 12,300 acres. These original records were adjusted by the COE in 1963 after reviewing information from a 1953 range system consisting of 71 monumented sedimentation and 11 degradation ranges. The revised storage at the normal pool elevation was estimated to be 456,884 acre-feet with a surface area of 12,416 acres. In 1961 a resurvey of Belton Lake was performed by the COE in which 26 of the sedimentation range lines were surveyed. The storage volume was calculated at elevation 594.0 to be 447,500 acre-feet with a surface area of 12,420 acres. In 1966 a re-survey was performed by the COE in which 37 of the original 71 sedimentation ranges and 3 of the 11 degradation ranges were surveyed. The storage volume was calculated at elevation 594.0 to be 441,984 acre-feet with a surface area of 12,423 acres.

HYDROGRAPHIC SURVEYING TECHNOLOGY

The following sections will describe the equipment and methodology used to conduct this hydrographic survey. Some of the theory behind Global Positioning System (GPS) technology and its accuracy are also addressed.

GPS Information

The following is a brief and simple description of Global Positioning System (GPS) technology. GPS is a new technology that uses a network of satellites, maintained in precise orbits around the earth, to determine locations on the surface of the earth. GPS receivers continuously monitor the broadcasts from the satellites to determine the position of the receiver. With only one satellite being monitored, the point in question could be located anywhere on a sphere surrounding the satellite with a radius of the distance measured. The observation of two satellites decreases the possible location to a finite number of points on a circle where the two spheres intersect. With a third satellite observation, the unknown location is reduced to two points where all three spheres intersect. One of these points is obviously in error because its location is in space, and it is ignored. Although three satellite measurements can fairly accurately locate a point on the earth, the minimum number of satellites required to determine a three dimensional position within the required accuracy is four. The fourth measurement compensates for any time discrepancies between the clock on board the satellites and the clock within the GPS receiver.

GPS technology was developed in the 1960s by the United States Air Force and the defense establishment. After program funding in the early 1970s, the initial satellite was launched on February 22, 1978. A four year delay in the launching program occurred after the Challenger space shuttle disaster. In 1989, the launch schedule was resumed. Full operational capability will be reached when the NAVSTAR (NAVigation System with Time And Ranging) satellite constellation is composed of 24 Block II satellites. At the time of the survey, the system had achieved initial operational capability. A full constellation of 24 satellites, in a combination of Block I (prototype) and Block II satellites, was fully functional. The NAVSTAR satellites provide data based on the World Geodetic System (WGS '84) spherical datum. WGS '84 is essentially identical to NAD '83.

The United States Department of Defense (DOD) is currently responsible for implementing and maintaining the satellite constellation. In an attempt to discourage the use of these survey units as a guidance tool by hostile forces, the DOD has implemented

means of false signal projection called Selective Availability (S/A). Positions determined by a single receiver when S/A is active result in errors to the actual position of up to 100 meters. These errors can be reduced to centimeters by performing a static survey with two GPS receivers, one of which is set over a point with known coordinates. The errors induced by S/A are time-constant. By monitoring the movements of the satellites over time (one to three hours), the errors can be minimized during post processing of the collected data and the unknown position computed accurately.

Differential GPS (DGPS) can determine positions of moving objects in real-time or "on-the-fly." One GPS receiver was set up over a benchmark with known coordinates established by the hydrographic survey crew. This receiver remained stationary during the survey and monitored the movements of the satellites overhead. Position corrections were determined and transmitted via a radio link once per second to a second GPS receiver located on the moving boat. The boat receiver used these corrections, or differences, in combination with the satellite information it received to determine its differential location. The large positional errors experienced by a single receiver when S/A is active are greatly reduced by utilizing DGPS. The reference receiver calculates satellite corrections based on its known fixed position, which results in positional accuracies within three meters for the moving receiver. DGPS was used to determine horizontal position only. Vertical information was supplied by the depth sounder.

Equipment

The equipment used in the performance of the hydrographic survey consisted of a 23-foot aluminum tri-hull SeaArk craft with cabin, equipped with twin 90-Horsepower Johnson outboard motors. Installed within the enclosed cabin are an Innerspace Helmsman Display (for navigation), an Innerspace Technology Model 449 Depth Sounder and Model 443 Velocity Profiler, a Trimble Navigation, Inc. 4000SE GPS receiver, a Motorola Radius radio with an Advanced Electronic Applications, Inc. packet modem, and an on-board computer. The computer was supported by a dot matrix printer and a

B-size plotter. Power was provided by a water-cooled generator through an in-line uninterruptible power supply. Reference to brand names does not imply endorsement by the TWDB.

The shore station included a second Trimble 4000SE GPS receiver, Motorola Radius radio and Advanced Electronic Applications, Inc. packet modem, and an omnidirectional antenna mounted on a modular aluminum tower to a total height of 40 feet. The combination of this equipment provided a data link with a reported range of 25 miles over level to rolling terrain that does not require that line-of-sight be maintained with the survey vessel in most conditions, thereby reducing the time required to conduct the survey.

As the boat traveled across the lake surface, the depth sounder gathered approximately ten readings of the lake bottom each second. The depth readings were averaged over the one-second interval and stored with the positional data to an on-board computer. After the survey, the average depths were corrected to elevation using the daily lake elevation. The set of data points logged during the survey were used to calculate the lake volume. Accurate estimates of the lake volume can be quickly determined using these methods to produce an affordable survey. The level of accuracy is equivalent to or better than previous methods used to determine lake volumes, some of which are discussed below.

Previous Survey Procedures

Originally, reservoir surveys were conducted with a rope stretched across the reservoir along pre-determined range lines. A small boat would manually pole the depth at selected intervals along the rope. Over time, aircraft cable replaced the rope and electronic depth sounders replaced the pole. The boat was hooked to the cable, and depths were again recorded at selected intervals. This method, used mainly by the Soil Conservation Service, worked well for small reservoirs.

Larger bodies of water required more involved means to accomplish the survey, mainly due to increased size. Cables could not be stretched across the body of water, so surveying instruments were utilized to determine the path of the boat. Monumentation was set for the end points of each line so the same lines could be used on subsequent surveys. Prior to a survey, each end point had to be located (and sometimes reestablished) in the field and vegetation cleared so that line of sight could be maintained. One surveyor monitored the path of the boat and issued commands via radio to insure that it remained on line while a second surveyor determined depth measurement locations by turning angles. Since it took a major effort to determine each of the points along the line, the depth readings were spaced quite a distance apart. Another major cost was the land surveying required prior to the reservoir survey to locate the range line monuments and clear vegetation.

Electronic positioning systems were the next improvement. If triangulation could determine the boat location by electronic means, then the boat could take continuous depth soundings. A set of microwave transmitters positioned around the lake at known coordinates would allow the boat to receive data and calculate its position. Line of site was required, and the configuration of the transmitters had to be such that the boat remained within the angles of 30 and 150 degrees in respect to the shore stations. The maximum range of most of these systems was about 20 miles. Each shore station had to be accurately located by survey, and the location monumented for future use. Any errors in the land surveying resulted in significant errors that were difficult to detect. Large reservoirs required multiple shore stations and a crew to move the shore stations to the next location as the survey progressed. Land surveying was still a major cost.

Another method used mainly prior to construction utilized aerial photography to generate elevation contours which could then be used to calculate the volume of the reservoir. Fairly accurate results could be obtained, although the vertical accuracy of the aerial topography was generally one-half of the contour interval or \pm five feet for a tenfoot contour interval. This method could be quite costly and was only applicable in areas

that were not inundated.

PRE-SURVEY PROCEDURES

The reservoir's surface area was determined prior to the survey by digitizing with AutoCad software the lake's normal pool boundary from six USGS quad sheets. The names of the quad sheets are as follows: Belton, TX, 1965 (Revised 1993); Bland TX, 1958 (Photo-revised 1978); Eagle Springs, TX, 1965 (Revised 1993); Leon Junction, TX, 1957 (Photo-revised 1978); Moffat, TX, 1965 (Revised 1993) and Nolanville, TX, 1958 (Photo-revised 1974).

The survey layout was designed by placing survey track lines at 500 foot intervals across the lake. The survey design for this lake required approximately 360 survey lines to be placed along the length of the lake. Survey setup files were created using Innerspace Technology Inc. software for each group of track lines that represented a specific section of the lake. The setup files were copied onto diskettes for use during the field survey.

SURVEY CONTROL SETUP

The first task of the Hydrographic Survey field staff after arriving at Belton Lake was to establish a horizontal reference control point. Due to the length of the lake, two control points were deemed necessary. Figure 3 shows the locations of the control points established. These locations were chosen due to their close proximity to the reservoir and the security of the areas.

Prior to the field survey, TWDB staff had researched locations of known firstorder benchmarks and requested Brazos River Authority employees to physically locate the associated monuments. Of the monuments found, the one chosen to provide horizontal control for the survey was a United States Geological Survey first-order

monument named BELTON 1943 located on the campus of the University of Mary Hardin Baylor in Belton, Texas. The coordinates for the monument are published as Latitude 31° 04' 04.19687"N and Longitude 97° 27' 53.89148"W.

On September 12, 1994 at the location for the first control point, staff set a standard surveying brass cap labeled TWDB #15 in concrete, flush to the ground. A static survey was performed from the BELTON 1943 monument to the control point using two Trimble 4000SE GPS receivers. The GPS receivers were setup on tripods over each point and satellite data were gathered for approximately one hour, with up to six satellites visible at the same time to the receivers. While maintaining the receiver at the BELTON 1943 monument, this procedure was repeated at the second control point labeled TWDB #16.

Once data collection ended, the data were retrieved and processed from both receivers, using Trimble Trimvec software, to determine coordinates for the control points. The WGS' 84 coordinates for TWDB #15 were determined to be North latitude 31° 07' 36.10491", West longitude 97° 31' 03.95891", with an ellipsoid height of 192.2163 meters. The approximate NGVD '29 elevation was 720.55 feet. The WGS' 84 coordinates for TWDB #16 were determined to be North latitude 31° 11' 49.98929", West longitude 97° 27' 32.68782", with an ellipsoid height of 189.2313 meters. The approximate NGVD '29 elevation was 711.17 feet.

Using the newly determined coordinates, a shore station was setup at TWDB #15 to provided DGPS control during the survey. The coordinates from the static survey were entered into the GPS receiver located over the control point to fix its location. Data received during the survey could then be corrected and broadcast to the GPS receiver on the moving boat during the survey.

SURVEY PROCEDURES

The following procedures were followed during the hydrographic survey of Belton Lake performed by the TWDB. Information regarding equipment calibration and operation, the field survey, and data processing is presented.

Equipment Calibration and Operation

During the survey, the GPS receivers were operated in the following DGPS modes. The reference station receiver was set to a horizontal mask of 0°, to acquire information on the rising satellites. A horizontal mask of 10° was used on the roving receiver for the purpose of calculating better horizontal positions. A PDOP (Position Dilution of Precision) limit of 7 was set for both receivers. The DGPS positions are known to be within acceptable limits of horizontal accuracy when the PDOP is seven (7) or less. An internal alarm sounds if the PDOP rises above seven to advise the field crew that the horizontal position has degraded to an unacceptable level.

Prior to the survey, TWDB staff verified the horizontal accuracy of the DGPS used during the Belton Lake survey to be within the specified accuracy of three meters by the following procedure. The shore station was set up over a known United States Geological Service (USGS) first order monument and placed in differential mode. The second receiver, directly connected to the boat with its interface computer, was placed over another known USGS first order monument and data was collected for 60 minutes in the same manner as during a survey. Based on the differentially-corrected coordinates obtained and the published coordinates for both monuments, the resulting positions fell within a three-meter radius of the actual known monument position.

At the beginning of each surveying day, the depth sounder was calibrated with the Innerspace Velocity Profiler. The Velocity Profiler calculates an average speed of sound through the water column of interest for a designated draft value of the boat (draft is the vertical distance that the boat penetrates the water surface). The draft of the boat was previously determined to average 1.2 ft. The velocity profiler probe is placed in the

water to moisten and acclimate the probe. The probe is then raised to the water surface where the depth is zeroed. The probe is lowered on a cable to just below the maximum depth set for the water column, and then raised to the surface. The unit displays an average speed of sound for a given water depth and draft, which is entered into the depth sounder. The depth value on the depth sounder was then checked manually with a measuring tape to ensure that the depth sounder was properly calibrated and operating correctly. During the survey of Belton Lake , the speed of sound in the water column varied daily between 4,916 and 4,926 feet per second. Based on the measured speed of sound for various depths, and the average speed of sound calculated for the entire water column, the depth sounder is accurate to within ± 0.2 feet, plus an estimated error of ± 0.3 feet due to the plane of the boat for a total accuracy of ± 0.5 feet for any instantaneous reading. These errors tend to be minimized over the entire survey, since some are plus readings and some are minus readings. Further information on these calculations is presented in Appendix A.

Field Survey

Data was collected on Belton Lake during the period of September 12-22, 1994. Approximately 105,920 data points were collected over the 215 miles traveled along the pre-planned survey lines and the random data-collection lines. These points were stored digitally on the boat's computer in 355 data files. Data were not collected in areas of shallow water (depths less than 3.0 ft.) or with significant obstructions unless these areas represented a large amount of water. Random data points were collected when determined necessary by the field crew by manually poling the depth and entering the depth value into the data file. As each point was entered, the DGPS horizontal position was stored automatically with each return keystroke on the computer. The boat was moving slowly during this period so positions stored were within the stated accuracy of \pm 3 meters to the point poled. Figure 2 shows the actual location of the data collection points.

Analog charts were printed for each survey line as the data were collected. The gate mark, which is a known distance above the actual depth, was also printed on the chart. Each chart was labeled with the date and data file ID for future reference. The depth sounder was set to record bad depth readings as 0.

The collected data were stored in individual data files for each pre-plotted range line or random data collection events. These files were downloaded to diskettes at the end of each day for further processing.

Data Processing

All collected data were down-loaded from diskettes onto the TWDB's computer network. The diskettes were then stored in a secured, safe location for future reference as needed. A Fortran program stripped the data collection files of non-essential data and created a Temporary data file. This data file consists of latitude, longitude and depth readings for each data point. The depth readings consist of instantaneous, average and auxiliary readings. The data files were edited manually by comparing the analog charts to the gate mark. Where the gate mark indicated that the recorded depth was other than the bottom, the depths were modified to reflect the recorded bottom. The Temporary files were then saved as Output files after editing was completed. The Output files were run through another Fortran program to delete all zero depth readings and to replace the average reading with the spot reading when the average reading was zero and the spot reading was greater then zero. The resulting file was saved as the final data file. Each of the individual data files were then combined into a single datacollection file that represented the date of data collection. The depths were then transformed to elevations with a simple Unix command based on the water surface elevation of each day. The elevations were rounded to the nearest tenth of a foot since the depth sounder records in tenths. The water surface ranged from 594.06 to 594.16 feet during the survey. Each of the daily files were then combined into a single edited data file to be used to develop a model of the lake's bottom surface.

The resulting DOS data file was imported into the UNIX operating system used to run Environmental Systems Research Institutes's (ESRI) Arc/Info GIS software. The latitude and longitude coordinates of each point were then converted to decimal degrees by a UNIX awk command. The awk command manipulates the data file format into a MASS points format for use by the GIS software. The graphic boundary file used for guidance along the pre-plotted survey lines was then transformed from NAD '27 datum to NAD '83, using Environmental Systems Research Institutes's (ESRI) Arc/Info project command with the NADCOM parameters. The area of the lake boundary was checked to verify that the area was the same in both datums. Once this was accomplished successfully, the boundary and the edited data file were in the same datum.

The two files are edited using the Arc/Edit module. The MASS points are converted into a point coverage and plotted on top of the boundary file. If data points were collected outside the boundary file, the boundary was modified to include the data points. The boundary near the edges of the lake in areas of significant sedimentation was down-sized to reflect the observations of the field crew. The resulting boundary shape was considered to be the acreage at the normal pool elevation of the lake. This was calculated as 12,385 acres for Belton Lake. The Board does not represent the boundary, as depicted in this report, to be a detailed actual boundary. Instead, it is a graphical approximation of the actual boundary used solely to compute the volume and area of the lake. The boundary does not represent the true land versus water boundary of the lake. An aerial topo of the upper four feet of the lake or an aerial photo taken when the lake is at the normal pool elevation would more closely define the present boundary. However, the minimal increase in accuracy does not appear to offset the cost of those services at this time.

The edited MASS points and modified boundary file were used to create a Digital Terrain Model (DTM) of the reservoir's bottom surface using Arc/Info's TIN module. The module builds an irregular triangulated network from the data points and the boundary file. This software uses a method known as Delauney's criteria for triangulation. A

triangle is formed between three non-uniformly spaced points, including all points along the boundary. If there is another point within the triangle, additional triangles are created until all points lie on the vertex of a triangle. All of the data points are preserved for use in determining the solution of the model by using this method. The generated network of three-dimensional triangular planes represents the actual bottom surface. Once the triangulated irregular network (TIN) is formed, the software then calculates elevations along the triangle surface plane by solving the equations for elevation along each leg of the triangle. Areas that were too shallow for data collection or obstructed by vegetation were estimated by the Arc/Info's TIN product using this method of interpolation.

There were some areas where values could not be calculated by interpolation because of a lack of information along the boundary of the reservoir. "Flat triangles" were drawn at these locations. Arc/Info does not use flat triangle areas in the volume or contouring features of the model. These areas were determined to be insignificant on Belton Lake. Therefore no additional points were required for interpolation and contouring of the entire lake surface. The TIN product calculated the surface area and volume of the entire reservoir at one-tenth of a foot intervals from the three-dimensional triangular plane surface representation. The computed reservoir volume table is presented in Appendix B and the area table in Appendix C. An elevation-area-volume graph is presented in Appendix D.

Other presentations developed from the model include a shaded relief map and a shaded depth range map. To develop the shaded relief map, the three-dimensional triangular surface was modified by a GRIDSHADE command. Colors were assigned to different elevation values of the grid. Using the command COLORRAMP, a set of colors that varied from navy to yellow was created. The lower elevation was assigned the color of navy, and the lake normal pool elevation was assigned the color of yellow. Different color shades were assigned to the different depths in between. Figure 4 presents the resulting depth shaded representation of the lake. Figure 5 presents a similar version of the same map, using bands of color for selected depth intervals. The color increases in intensity from the shallow contour bands to the deep water bands.

The DTM was then smoothed and linear smoothing algorithms were applied to the smoothed model to produce smoother contours. The resulting contour map of the bottom surface at ten-foot intervals is presented in Figure 6.

RESULTS

Staff of the TWDB collected hydrographic data on Belton Lake during the period September 12-22, 1994. The survey crew observed that the widest area of the lake was at the confluence of Cowhouse Creek and the Leon River. The Leon River segment of Belton Lake was observed to have river characteristics with major relief along the perimeter. As the river meandered through the limestone rock terrain, the survey crew observed shallow silt deposit banks on one side and a deep cut channel on the opposite side. The width of the river channel varied between 1/4 and 1/2 mile from the confluence of Cowhouse Creek to the Highway 36 bridge on the Leon River. Upstream of the Highway 36 bridge, the terrain became more gentle with rolling hills and a wider flood plain. The Cowhouse Creek arm exhibited similar characteristics to the terrain above the Highway 36 bridge.

Results from the survey indicate Belton Lake now encompasses around 12,385 surface acres and contains a volume of 434,500 acre-feet at the normal pool elevation of 594.0 feet. The lowest elevation encountered during the field survey was 481.46 feet, or 112.54 feet of depth and was found near the dam.

The storage volume calculated by this survey is approximately 1.7 percent less than the 1966 previous record information for the lake. The lowest gated outlet invert elevation is at elevation 483.0 feet. There is no dead storage volume in the lake below this elevation. Therefore, the conservation storage capacity is calculated to be 434,500 acre-feet. Since the maximum depth of the lake is within 1.5 ft of the lowest gated outlet, the potential for the outlet to become silted in exists in the near future.

Operational procedures should be considered and implemented to maintain the functionality of the outlet.

SUMMARY

When Belton Lake was built in 1954, it was estimated to contain 457,000 acrefeet of water at the normal pool elevation of 594.0 ft. This original estimate was revised to 456,884 acre-feet after a sedimentation range line network was established in 1953-54. In 1961, a sedimentation survey of Belton Lake performed by US Army Corps of Engineers (COE) reported the new volume of the lake to be 447,500 acre-feet at the normal pool elevation. In 1966, the lake was again surveyed by the COE and the volume was revised to 441,984 acre-feet. The COE estimated that Belton Lake had accumulated 9,733 acre-ft of sediment between 1949 and 1961, and an additional 5,122 acre-feet of sediment between 1961 and 1966. The average annual sediment accumulation rate for the period 1949-61 was estimated at 1,269 acre-feet. The average annual sediment accumulation rate for the period 1961-66 was estimated at 1,024 acre-feet.

In September 1994, a hydrographic survey of Belton Lake was performed by the Texas Water Development Board's Hydrographic Survey Program. The 1994 survey used technological advances such as differential global positioning system and geographical information system technology to build a model of the reservoir's bathemetry. These advances allowed a survey to be performed quickly and to collect significantly more data of the bathemetry of Belton Lake than the previous surveys. Results from the survey indicate that the lake's capacity and conservation storage capacity at the normal pool elevation of 594.0 feet was 434,500 acre-feet. The estimated reduction in storage capacity, if compared to the 1966 survey information, was 7,484 acre-feet, or 1.7 percent. This equates to an estimated loss of 267.29 acre-feet per year during the 28 years between the TWDB's survey and the last survey performed by the COE.

It is difficult to compare the surveys performed by the TWDB and the COE because the methods and procedures used were very different. However, the TWDB considers the 1994 survey to be a significant improvement over previous survey procedures and recommend that the same methodology be used to re-surveyed Belton Lake in five to ten years or after major flood events. A second survey will remove any noticeable error due to improved calculation techniques and will isolate current sedimentation rates and the storage losses occurring in Belton Lake.

CALCULATION OF DEPTH SOUNDER ACCURACY

This methodology was extracted from the Innerspace Technology, Inc. Operation Manual for the Model 443 Velocity Profiler.

t = (D - d)/VFor the following examples,

> where: t_D = travel time of the sound pulse, in seconds (at depth = D) D = depth, in feet d = draft = 1.2 feet V = speed of sound, in feet per second

To calculate the error of a measurement based on differences in the actual versus average speed of sound, the same equation is used, in this format: D

$$0 = [t(V)] + d$$

For the water column from 2 to 30 feet: V = 4832 fps

 $t_{30} = (30-1.2)/4832$ = 0.00596 sec.

For the water column from 2 to 45 feet: V = 4808 fps

 $t_{45} = (45 - 1.2)/4808$ =0.00911 sec.

For a measurement at 20 feet (within the 2 to 30 foot column with V = 4832 fps):

 $D_{20} = [((20-1.2)/4832)(4808)]+1.2$ = 19.9' (-0.1')

For a measurement at 30 feet (within the 2 to 30 foot column with V = 4832 fps):

$$D_{30} = [((30-1.2)/4832)(4808)]+1.2 \\ = 29.9' \quad (-0.1')$$

For a measurement at 50 feet (within the 2 to 60 foot column with V = 4799 fps):

$$D_{50} = [((50-1.2)/4799)(4808)]+1.2 \\ = 50.1' (+0.1')$$

For the water column from 2 to 60 feet: V = 4799 fps Assumed $V_{80} = 4785$ fps

t₆₀ =(60-1.2)/4799 =0.01225 sec.

For a measurement at 10 feet (within the 2 to 30 foot column with V = 4832 fps):

$$D_{10} = [((10-1.2)/4832)(4799)]+1.2 = 9.9' (-0.1')$$

For a measurement at 30 feet (within the 2 to 30 foot column with V = 4832 fps):

$$D_{30} = [((30-1.2)/4832)(4799)]+1.2 = 29.8' (-0.2')$$

For a measurement at 45 feet (within the 2 to 45 foot column with V = 4808 fps):

$$D_{45} = [((45-1.2)/4808)(4799)]+1.2 = 44.9' (-0.1')$$

For a measurement at 80 feet (outside the 2 to 60 foot ∞ lumn, assumed V = 4785 fps):

 $D_{80} = [((80-1.2)/4785)(4799)]+1.2$ = 80.2' (+0.2')

TEXAS WATER DEVELOPMENT BOARD RESERVOIR VOLUME TABLE

		VOLUME IN	ACRE-FEET			ELEVAT	ION INCREME	NT IS ONE 1	ENTH FOOT	
ELEV. FEET	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	23128	28.1.1.2	54212							
481										
482										
483										1
484	CT-STORE 1	1	1	1	1	1	1	1	1	1
485	2	2	2	2	2	2	3	3	3	3
486	3	4	4	4	5	5	5	6	6	7
487	7	8	9	10	10	11	12	13	14	15
488	16	17	18	19	20	22	23	24	26	27
489	29	31	32	34	36	38	40	42	44	47
490	49	51	54	56	59	61	64	66	69	72
491	75	78	81	84	87	90	93	97	100	104
492	107	111	114	118	122	126	130	134	138	142
493	147	151	156	161	166	171	176	181	186	192
494	197	203	209	215	221	228	234	241	248	255
495	262	269	276	284	291	299	307	315	324	332
496	341	350	359	369	378	388	397	407	417	428
497	438	448	459	470	481	492	503	514	526	538
498	549	561	573	586	598	611	624	637	650	663
499	676	690	704	718	732	747	761	776	791	807
500	822	838	854	870	887	904	921	938	955	973
501	991	1010	1028	1048	1067	1087	1107	1128	1149	1170
502	1192	1214	1237	1260	1283	1307	1331	1355	1380	1405
503	1431	1457	1483	1510	1537	1564	1591	1619	1648	1676
504	1705	1735	1764	1794	1824	1855	1886	1917	1949	1981
505	2013	2045	2078	2112	2145	2179	2214	2249	2284	2319
506	2355	2391	2427	2464	2501	2539	2577	2615	2654	2693
507	2733	2772	2813	2853	2894	2936	2977	3020	3062	3105
508	3148	3192	3236	3281	3325	3371	3416	3462	3509	3555
509	3603	3650	3698	3747	3795	3845	3894	3944	3995	4046
510	4097	4149	4201	4254	4307	4361	4415	4469	4524	4580
511	4636	4692	4749	4807	4865	4924	4983	5043	5103	5164
512	5226	5288	5350	5414	5477	5542	5606	5672	5738	5804
513	5871	5939	6007	6075	6145	6214	6285	6356	6427	6499
514	6572	6645	6719	6794	6869	6944	7021	7097	7175	7253
515	7332	7411	7491	7572	7653	7735	7817	7901	7985	8070
516	8156	8242	8330	8419	8508	8598	8690	8782	8875	8969
517	9064	9160	9256	9354	9452	9551	9652	9753	9855	9957
518	10061	10166	10271	10377	10484	10592	10701	10811	10922	11033
519	11145	11258	11372	11486	11602	11718	11835	11953	12072	12192
520	12312	12433	12555	12678	12802	12926	13052	13178	13305	13433
521	13562	13691	13822	13953	14085	14218	14352	14486	14622	14758
522	14895	15033	15172	15311	15451	15592	15734	15876	16019	16163
	16307	16452	16598	16745	16892	17040	17188	17338	17488	17638
523		17942	18095	18248	18403	18558	18713	18870	19027	19185
524	17790 19343	19502	19662	19822	19983	20145	20307	20470	20633	20797
525		21128	21294	21461	21628	21796	21965	22135	22306	22477
526	20962		22994	23168	23342	23517	23693	23870	24047	24224
527	22649	22821		24943	25124	25306	25488	25672	25856	26041
528	24403	24582	24762		26978	27168	27358	27550	27742	27935
529	26227	26413	26601	26789	207/0	21100	21330	21330	21146	

					EI EVA	TION INCREM	ENT IS ONE	TENTH FOOT	
	VOLUME IN				100 C 100				.9
FEET .0	.1	.2	.3	-4	.,	.0			
202000	297920	284760	285710	286660	287610	288560	289510	290470	291420
and the second second			A CONTRACTOR OF A CONTRACTOR OF	296240	297210	298190	299160	300140	301110
and the second se	A CONTRACTOR OF THE				307030	308020	309010	310010	311010
Chinese Lawrence	and the second sec	Concernance of the second		The comprision is		318050	319070	320080	321100
				The second second second	and an an an and a loss	328290	329320	330360	331400
and the second second second	and the second second second second			17 17 17 19 19 19 19 19 19 19 19 19 19 19 19 19			339780	340830	341890
	a standard and a stand					and the second second		351510	352590
342950		The second second second		Contraction and the		- (T. 31 B.C.)			363480
353670	354750	and the second second						and the second sec	374590
364580	365680	366790	367900			and the particular of the			385910
375710	376840	377960	379090	380220					
387050	388200	389340	390490	391640	392800	393950	TO. 19670. 3 121.20		397430
	399770	400940	402120	403290	404470	405650	406830	408010	409200
		412770	413960	415150	416350	417550	418750	419950	421150
		and the second second	425980	427190	428400	429620	430830	432050	433270
and the second se	425500								
	282880 292380 302090 312010 322120 332440 342950 353670 364580 375710	.0 .1 282880 283820 292380 293350 302090 303080 312010 313010 322120 323140 332440 333480 342950 344010 353670 354750 364580 365680 375710 376840 387050 388200 398600 399770 410390 411580 422350 423560	282880 283820 284760 292380 293350 294310 302090 303080 304060 312010 313010 314010 322120 323140 324170 332440 333480 334520 342950 344010 345080 353670 354750 355830 364580 365680 366790 375710 376840 377960 387050 388200 389340 398600 399770 400940 410390 411580 412770 422350 423560 424770	FEET .0 .1 .2 .3 282880 283820 284760 285710 292380 293350 294310 295280 302090 303080 304060 305050 312010 313010 314010 315020 322120 323140 324170 325190 332440 333480 334520 335570 342950 344010 345080 346150 353670 354750 355830 356920 364580 365680 366790 367900 375710 376840 377960 379090 387050 388200 389340 390490 398600 399770 400940 402120 410390 411580 412770 413960 422350 423560 424770 425980	FEET .0 .1 .2 .3 .4 282880 283820 284760 285710 286660 292380 293350 294310 295280 296240 302090 303080 304060 305050 306040 312010 313010 314010 315020 316030 322120 323140 324170 325190 326220 332440 333480 334520 335570 336620 342950 344010 345080 346150 347210 353670 354750 355830 356920 358010 364580 365680 366790 367900 36920 375710 376840 377960 379090 380220 387050 388200 389340 390490 391640 398600 399770 400940 402120 403290 410390 411580 412770 413960 415150 422350 423560 424770 4259	FEET .0 .1 .2 .3 .4 .5 282880 283820 284760 285710 286660 287610 292380 293350 294310 295280 296240 297210 302090 303080 304060 305050 306040 307030 312010 313010 314010 315020 316030 317040 322120 323140 324170 325190 326220 327250 332440 333480 334520 335570 336620 337670 342950 344010 345080 346150 347210 348280 353670 354750 355830 356920 358010 359100 364580 365680 366790 367900 369010 370120 375710 376840 377960 379090 380220 381360 387050 388200 389340 390490 391640 392800 398600 399770 400940 <	FEET .0 .1 .2 .3 .4 .5 .6 282880 283820 284760 285710 286660 287610 288560 292380 293350 294310 295280 296240 297210 298190 302090 303080 304060 305050 306040 307030 308020 312010 313010 314010 315020 316030 317040 318050 322120 323140 324170 325190 326220 327250 328290 332440 333480 334520 335570 336620 337670 338720 342950 344010 345080 346150 347210 348280 349360 353670 354750 355830 356920 358010 359100 360190 364580 365680 366790 367900 369010 370120 371230 375710 376840 377960 379090 380220 381360 382490	FEET .0 .1 .2 .3 .4 .5 .6 .7 282880 283820 284760 285710 286660 287610 288560 289510 292380 293350 294310 295280 296240 297210 298190 299160 302090 303080 304060 305050 306040 307030 308020 309010 312010 313010 314010 315020 316030 317040 318050 319070 322120 323140 324170 325190 326220 327250 328290 329320 332440 333480 334520 335570 336620 337670 338720 339780 342950 344010 345080 346150 347210 348280 349360 350430 353670 354750 355830 356920 358010 359100 360190 361290 364580 366580 366790 367900 380220 381360	FEET .0 .1 .2 .3 .4 .5 .6 .7 .8 282880 283820 284760 285710 286660 287610 288560 289510 290470 292380 293350 294310 295280 296240 297210 298190 299160 300140 302090 303080 304060 305050 306040 307030 308020 309010 310010 312010 313010 314010 315020 316030 317040 318050 319070 320080 322120 323140 324170 325190 326220 327250 328290 329320 330360 332440 333480 334520 335570 336620 337670 338720 339780 340830 342950 344010 345080 346150 347210 348280 349360 350430 351510 353670 354750 355830 356920 358010 359100 360190

TEXAS WATER DEVELOPMENT BOARD RESERVOIR AREA TABLE

		AREA IN AC	RES			ELEVAT	ION INCREME	NT IS ONE T	ENTH FOOT	
ELEV. FEET	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
481										
482										
483								1	381	1
484	- 1	2231	271	1	2331	1	1	1.754	1	1
485	1	-34.1	2	2	2	2	2	2	2	2
486	3	3	3	3	4	4	3.4	5	5	6
487	6	7	7	8	8	8	9	9	10	10
488	10	11	11	12	12	13	14	14	15	15
489	16	17	18	19	19	20	21	21	22	22
490	23	24	24	25	25	26	27	27	28	28
491	29	30	30	31	32	32	33	34	34	35
492	36	36	37	38	39	40	41	41	42	43
493	- 44	46	47	48	49	50	52	53	55	56
494	57	59	60	61	63	64	66	67	68	70
495	71	73	74	76	78	79	81	83	85	86
496	88	90	92	94	95	97	98	100	101	103
497	104	106	107	109	110	111	113	114	116	117
498	119	120	122	124	125	127	129	130	132	134
499	136	138	140	142	144	146	148	150	152	154
500	157	159	161	164	166	169	171	174	177	180
501	182	186	189	192	196	201	205	209	213	216
502	220	223	227	231	235	238	242	246	250	254
503	257	261	265	268	271	275	278	281	285	288
504	291	294	298	301	304	307	311	314	318	321
505	325	328	332	335	338	342	345	349	352	356
506	359	363	367	370	374	378	381	385	389	393
507	397	401	404	408	412	416	420	423	427	431
508	435	439	443	446	450	454	458	462	466	470
509	474	478	482	486	490	495	499	503	508	512
510	516	520	525	529	533	538	543	547	552	557
511	562	568	573	578	584	590	596	601	607	612
512	618	624	629	635	640	646	651	656	662	667
513	673	678	684	689	695	700	706	712	718	724
514	731	737	742	748	753	759	765	771	778	784
515	790	797	803	810	816	823	830	837	844	853
516	863	873	881	890	900	908	917	926	935	944
517	953	962	971	980	988	997	1006	1015	1024	1033
518	1041	1050	1059	1067	1076	1084	1093	1101	1109	1118
519	1126	1134	1142	1150	1159	1167	1175	1183	1192	1200
520	1208	1216	1224	1233	1241	1249	1258	1267	1275	1284
521	1292	1300	1308	1317	1325	1334	1342	1350	1358	1366
522	1374	1383	1391	1398	1406	1413	1420	1427	1434	1441
523	1448	1455	1462	1469	1475	1482	1489	1496	1503	1510
524	1517	1525	1532	1539	1546	1554	1561	1568	1575	1581
525	1588	1594	1600	1607	1613	1619	1625	1631	1638	1644
526	1651	1658	1665	1672	1679	1687	1694	1701	1708	1715
527	1721	1728	1734	1741	1748	1754	1761	1768	1775	1782
528	1789	1796	1802	1809	1816	1823	1830	1838	1846	1854
529	1862	1870	1878	1886	1894	1901	1909	1917	1925	1933

ELRV. FEET .0 .1 .2 .3 .4 .5 .6 .7 .8 .9 330 1941 1949 1956 1964 1972 1980 1988 1996 2005 2013 331 2021 2030 2033 2047 2056 2067 2003 2092 2101 332 2100 2118 2218 2239 2249 2259 2230 2203 2041 2417 334 2312 2324 2335 2440 2516 2370 2607 2617 2462 2491 2512 2527 355 2333 2442 2354 2566 2656 2675 2766 2566 2597 2607 2607 2607 2607 2608 2694 2744 2714 2744 2714 2744 2714 2744 2714 2744 2714 2724 2936 2307 3008 3007 3007 3007			AREA IN AC	RES			ELEVATION INCREMENT IS ONE TENTH FOOT				
531 2021 2030 2033 2047 2055 2074 2083 2002 2110 532 2110 2119 2129 2138 2148 2157 2167 2176 2176 2176 2176 2176 2176 2181 2280 2291 2201 2301 2512 2522 2536 2570 2281 2591 2512 2522 536 2533 2543 2554 2566 2575 2685 2597 2601 2714 2724 538 2734 2745 2755 2755 2675 2685 2979 2603 2819 2819 540 2691 2071 2844 2869 2001 2013 2924 2926 2976 2604 3775 3064 3077 3064 3077 3064 3373 3344 3396 3407 3419 543 3511 3644 3577 3500 3002 3015 <t< th=""><th>ELEV. FEET</th><th>.0</th><th>.1</th><th>.2</th><th>.3</th><th>.4</th><th></th><th></th><th></th><th></th><th>.9</th></t<>	ELEV. FEET	.0	.1	.2	.3	.4					.9
531 2021 2030 2038 2077 2056 2065 2074 2083 2002 2101 532 2110 2119 2129 2139 2148 2157 2167 2176 2180 2291 2201 534 2217 2218 2228 2249 2259 2270 2281 2291 2201 535 2248 2239 2247 2285 2566 2576 2566 2577 2601 2712 2227 536 2253 2545 2566 2576 2266 2704 2714 2724 2747 2085 2819 2831 537 2642 2854 2666 2878 2889 2901 2913 2926 2936 2949 2931 2936 2949 2936 2949 3061 3077 3068 3171 3163 3147 3193 3171 3163 3147 3196 33171 3172 3141 <	530	1941	1949	1956	1964	1972	1980	1988	1996	2005	2013
532 2110 2119 2129 2133 2148 2157 2167 2176 2176 2176 2180 2201 533 2207 2218 2228 2239 2249 2259 2270 2280 2201 2301 534 2312 2224 2335 2357 2364 2257 2366 2577 2366 2577 2566 2577 2566 2577 2566 2577 2566 2577 2566 2577 2568 2377 2608 2819 2831 539 22642 2854 2666 2878 2369 2011 2013 2024 2026 2049 540 2061 2073 2064 2077 3009 3020 3033 3045 3057 3062 541 3000 3001 3114 3125 3136 3126 3136 3128 3364 3361 3316 3328 3329 3316 3328 <	531	2021	2030								
333 2207 2218 2229 2249 2259 2270 2280 2291 2301 334 2312 2324 2335 2347 2358 2370 2381 2393 2464 2417 2462 2411 2401 2401 2401 2402 2411 2402 2411 2402 2417 2462 2417 2462 2417 2462 2417 2462 2417 2462 2417 2462 2417 2462 2417 2462 2417 2462 2417 2462 2417 2462 2417 2462 2417 2462 2417 2426 2464 2456 2666 2767 2608 2819 2831 3313 3045 3057 3068 3013 3045 3057 3068 3013 3045 3057 3068 3047 3119 3143 3143 3143 3143 3143 3143 3143 3143 3143 3133 3137 3346											
534 2312 2324 2335 2347 2358 2370 2381 2393 2404 2417 535 2428 2439 2450 2461 2471 2482 2491 2501 2512 2522 537 2637 2646 2656 2675 2666 2677 2607 2607 2617 2627 538 2374 2775 2755 2755 2755 2755 2765 2777 2868 2899 2911 2913 2924 2936 2949 500 3003 3045 3057 3069 3020 3033 3045 3057 3046 2949 3041 3163 3174 3159 3164 3364 3366 3071 3111 3163 3374 3344 3366 3073 3344 3366 3073 3364 3366 3373 3349 3361 3376 3344 3376 3344 3376 3344 3376 3344	533										
535 2428 2439 2450 2441 2471 2482 2491 2501 2512 2522 536 2533 2543 2543 2546 2576 2586 2597 2607 2617 2247 538 2744 2745 2755 2775 2786 2797 2080 2819 2333 540 2961 2973 2964 2997 3009 3020 3033 3045 3057 3068 541 3080 3091 3102 3114 3125 3134 3147 3159 3171 3162 543 3313 3325 3337 3349 3361 3373 3364 3366 3607 3419 544 3431 3443 3453 3467 3528 3564 3558 3566 3568 3579 3668 3578 3566 3668 3679 3724 3796 3409 3939 3954 3668 36	534										
536 2533 2543 2554 2566 2676 2586 2597 2607 217 2627 537 2637 2646 2655 2665 2675 2685 2694 2774 2774 2775 2786 2777 2808 2819 2811 2813 3164 3164 3165 3164 3157 3364 3364 3067 3111 3185 543 3313 3325 3373 3364 3667 3373 3344 3657 3663 3610 3652 3641 3655 3656 544 3433 3552 3864 3881 3894 3090 3924 3939 3954 546	535										
537 2647 2646 2656 2675 2685 2694 2704 2714 2724 538 2734 2745 2755 2755 2775 2786 2777 2288 2819 2283 2894 2864 2897 3009 3023 3045 3057 3068 541 3080 3091 3102 3114 3125 3136 3147 3159 3171 3183 542 3194 3205 3216 3227 3242 3254 3266 3278 3302 3302 543 3313 3325 3337 349 3511 3374 3364 3366 3407 3158 544 3433 3452 3560 3602 3615 3628 3528 3539 3564 3668 3782 3796 3010 547 3824 3838 3852 3660 3881 3894 3909 3924 3939 3954 <	536										
538 274 2745 2755 2765 2775 2786 2797 2808 2819 2831 539 2842 2854 2864 2973 2889 2001 2013 3024 2054 2974 2986 2974 2986 2975 3069 3005 3057 3068 3057 3068 3057 3054 3157 3154 3147 3159 3171 3163 543 3313 3325 3337 3347 3540 3402 3544 3516 3528 3535 544 3431 3443 3455 3467 3480 3492 3548 3566 3681 3568 3477 3566 3681 3678 3776 3560 3668 3782 3796 3600 544 3683 3678 3771 3570 4606 4077 4076 4089 4103 544 3683 3678 3771 3586 3677 <td< td=""><td>537</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	537										
539 2642 2854 2866 2878 2889 2901 2913 2924 2936 2949 540 2961 2973 2984 2997 3009 3020 3033 3045 3057 3064 541 3080 3012 3114 3125 3136 3147 3159 3171 3181 3125 3337 3349 3361 3373 3384 3364 3364 3364 3365 3366 3407 3419 544 3431 3443 3455 3467 3400 3402 3564 3564 3528 3564 3563 3681 3572 3766 3810 547 3824 3383 352 3860 3881 3872 3768 31713 3771 3741 3755 3768 3779 3976 3610 544 3669 3984 4000 4015 4031 4046 4060 4075 4498 4171 <t< td=""><td>538</td><td>2734</td><td>2745</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	538	2734	2745								
540 261 2073 2084 2997 3009 3020 3033 3045 3057 3068 541 3080 3091 3102 3114 31125 31136 3147 3159 3171 3183 543 3313 3325 3337 3349 3361 3373 3384 3396 3407 3419 544 3431 3443 3455 3467 3601 3628 3641 3655 3566 3564 3577 3564 3577 3564 3577 3564 3577 3564 3681 3628 3641 3655 3668 3681 3699 3764 3099 3764 3099 3764 3669 3681 3699 3984 4000 4015 4031 4046 4060 4075 4089 4103 548 3969 3984 4000 4015 4031 4046 4477 4491 4506 4224 4224 4224	539	2842				and the second s					
541 3080 3091 3102 3114 3125 3136 3147 3159 3171 3183 542 3194 3205 3226 3224 3224 3226 32278 3200 3302 543 33313 3325 3337 3349 3361 3373 3344 3366 3077 3410 3402 3504 3516 3528 3539 545 3551 3564 3564 3688 377 3500 3602 3615 3628 3579 3668 3773 3727 3741 3755 3768 3782 3796 3661 547 3824 3838 3852 3866 3881 3894 3909 3924 4023 4046 4060 4075 4089 4103 549 4118 4133 4148 4131 4344 4331 4344 4355 4664 4655 4664 4655 4664 4655 4664 <	540										
542 3194 3205 3216 3227 3242 3254 3266 3278 3290 3302 543 3313 3325 3337 3349 3361 3373 3346 3366 3407 3419 544 3431 3443 3455 3467 3460 3402 3564 3561 3658 3641 3655 3668 545 3551 3564 3577 3590 3602 3615 3628 3641 3655 3668 546 3683 3698 3713 3727 3741 3755 3766 3762 3796 3810 547 3824 3838 4852 4664 4064 4060 4075 4089 4103 548 3969 3984 4000 4015 4031 4346 4458 426 4276 4220 4234 4248 4551 4456 4523 550 4522 4555 4569 <td>541</td> <td>3080</td> <td>3091</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>And in the Owner, which the</td>	541	3080	3091								And in the Owner, which the
543 3313 3325 3337 3349 3361 3373 3384 3396 3407 3419 544 3431 3443 3455 3667 3400 3492 3564 3576 3528 3539 545 3531 3564 3577 3590 3602 3615 5628 3641 3655 3668 546 3633 3698 3713 3727 3741 3755 3768 3782 3796 3810 547 3824 3838 3852 3866 3881 3894 3909 3924 3939 3954 548 3999 39944 4000 4015 4014 4184 4183 4148 4186 4318 4311 4344 4355 4569 418 43131 4344 4355 4664 4664 4558 551 4539 4555 4666 4602 4703 4714 4725 4736 4768 5	542	3194	3205								
544 3431 3443 3455 3467 3480 3492 3504 3516 3528 3539 545 3551 3564 3577 3590 3602 3615 3628 3641 3655 3668 547 3824 3838 3852 3866 3881 3894 3909 3924 3939 3954 548 3969 3984 4000 4015 4031 4046 4060 4075 4089 4103 549 4118 4133 4148 4163 4178 4192 4207 4224 4248 550 4262 4276 4290 4318 4331 4344 4358 4371 4385 551 4359 4455 4657 4656 4606 4072 4246 4466 4655 553 4669 4698 4592 4703 4714 4726 4736 4768 554 4779 4790 4801 4612 4623 4833 4944 4655 4665 4075	543	and the second s									
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		9209	9232				9312				

RESERVOIR AREA TABLE

page 3

		AREA IN A	CRES			ELEVA	ELEVATION INCREMENT		TENTH FOOT	
ELEV. I	FEET .O	.1	.2	.3	.4	.5	.6	.7	.8	.9
580	9407	9429	9448	9467	9487	9506	9526	9547	9567	9587
581	9608	9629	9650	9670	9690	9710	9730	9749	9768	9788
582	9809	9831	9852	9873	9893	9913	9933	9952	9973	9993
583	10014	10034	10054	10074	10094	10115	10135	10156	10176	10197
584	10216	10237	10257	10277	10296	10316	10335	10355	10374	10394
585	10414	10435	10455	10475	10495	10516	10536	10556	10575	10595
586	10615	10635	10655	10674	10694	10714	10735	10755	10775	10794
587	10814	10834	10854	10874	10894	10915	10936	10957	10978	10998
588	11019	11040	11062	11083	11106	11132	11155	11177	11198	11219
589	11239	11259	11279	11299	11319	11338	11358	11379	11399	11419
590	11439	11459	11480	11501	11523	11547	11571	11596	11621	11645
591	11671	11701	11735	11755	11773	11790	11808	11826	11843	11861
592	11878	11896	11913	11931	11948	11966	11984	12002	12020	12037
593	12055	12072	12090	12107	12125	12142	12159	12177	12194	12212
594	12385	1000 CT							12174	ILLIE

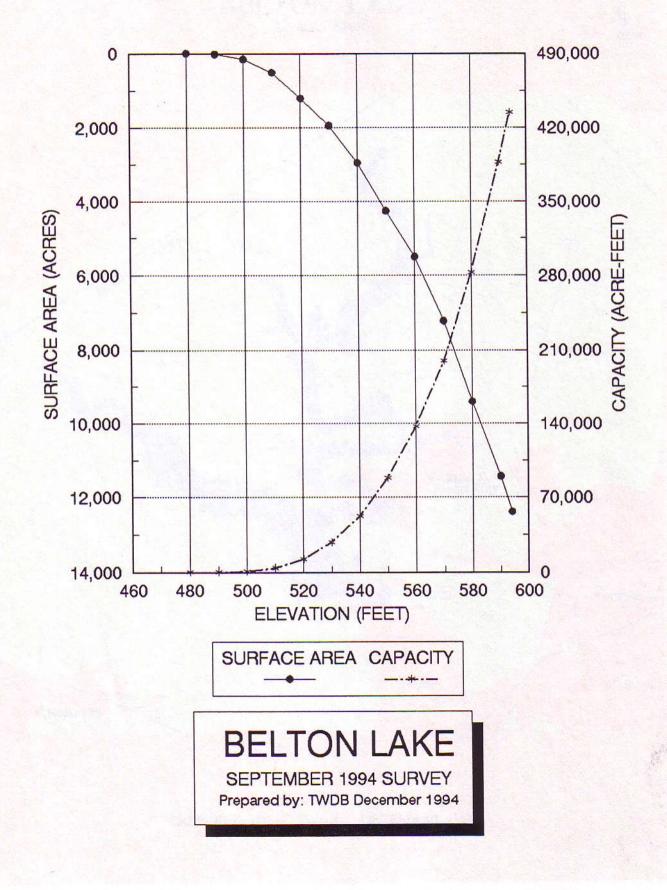
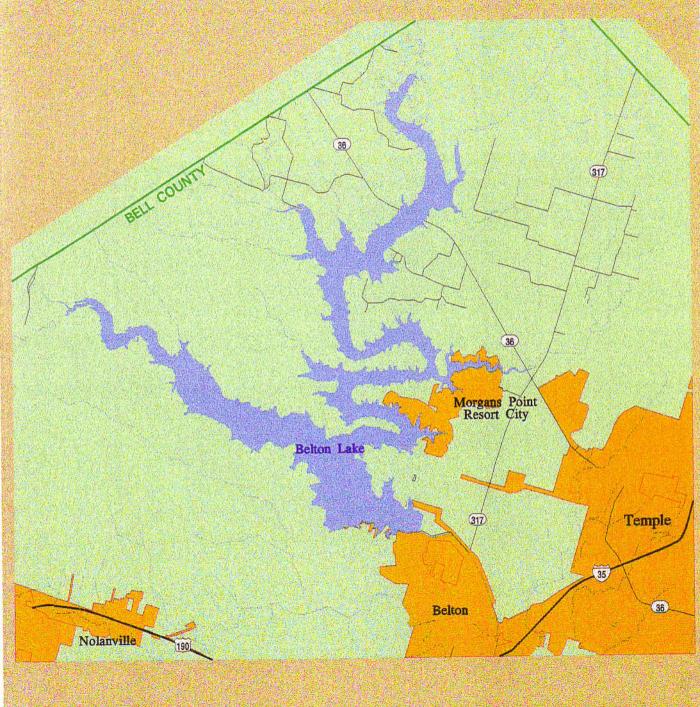


FIGURE 1

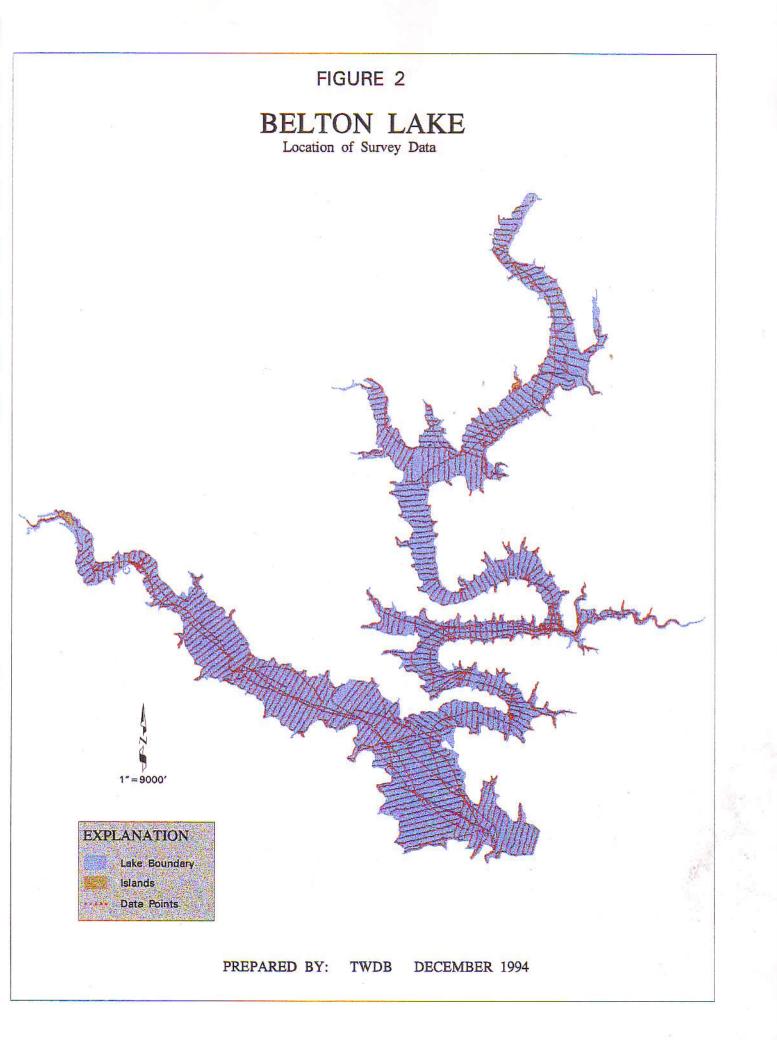
BELTON LAKE

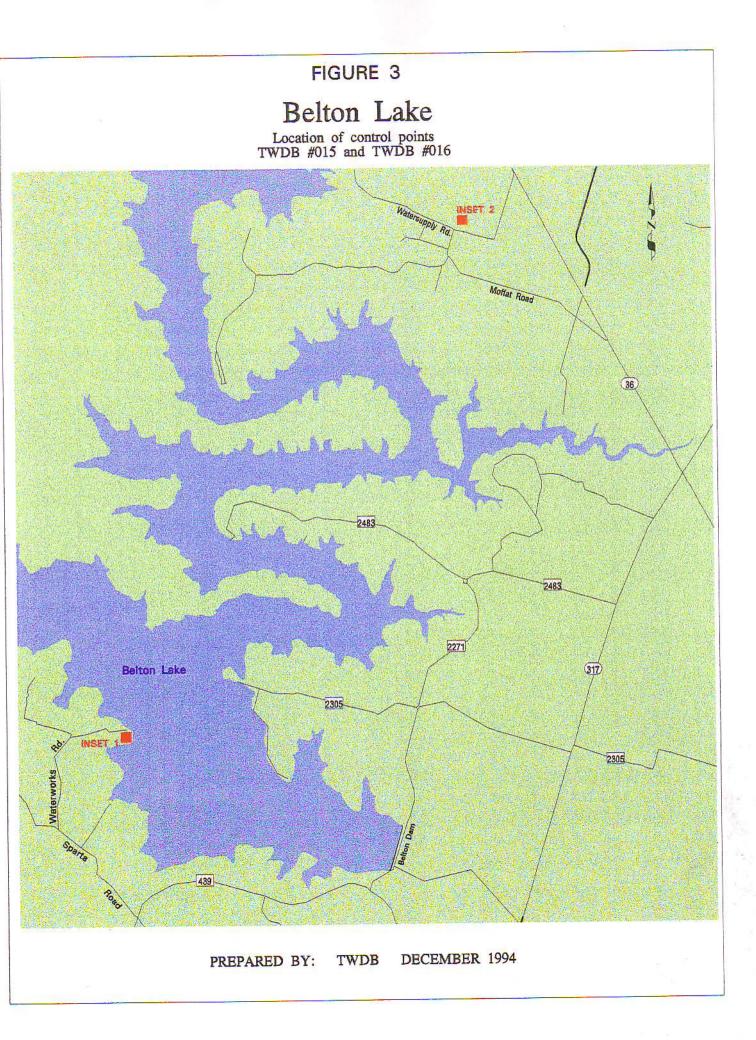
Location Map

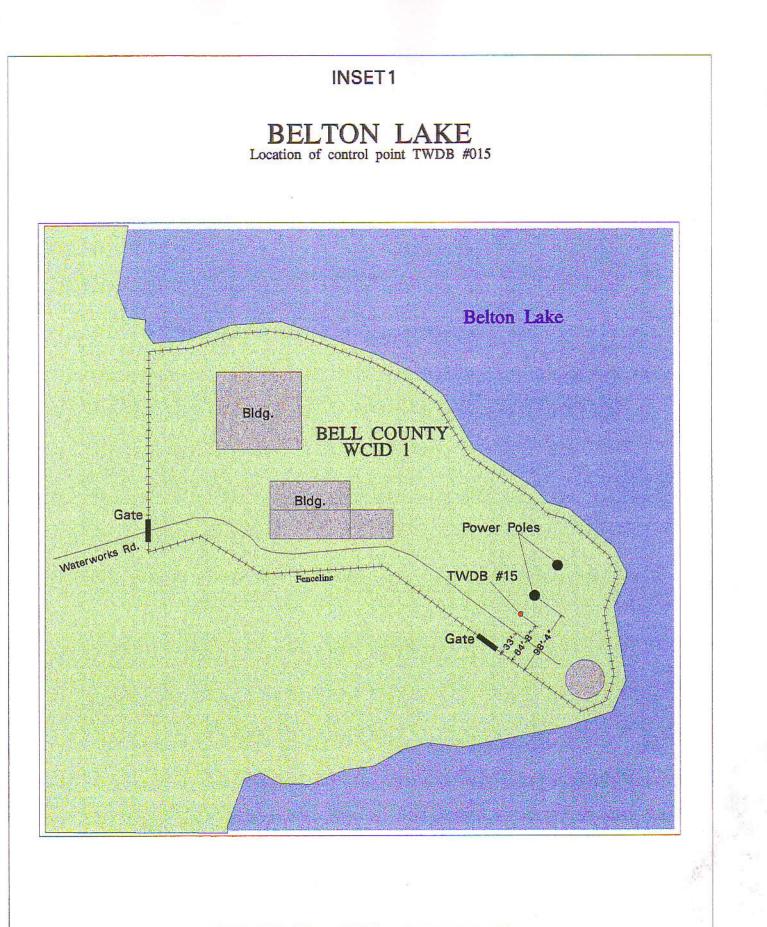




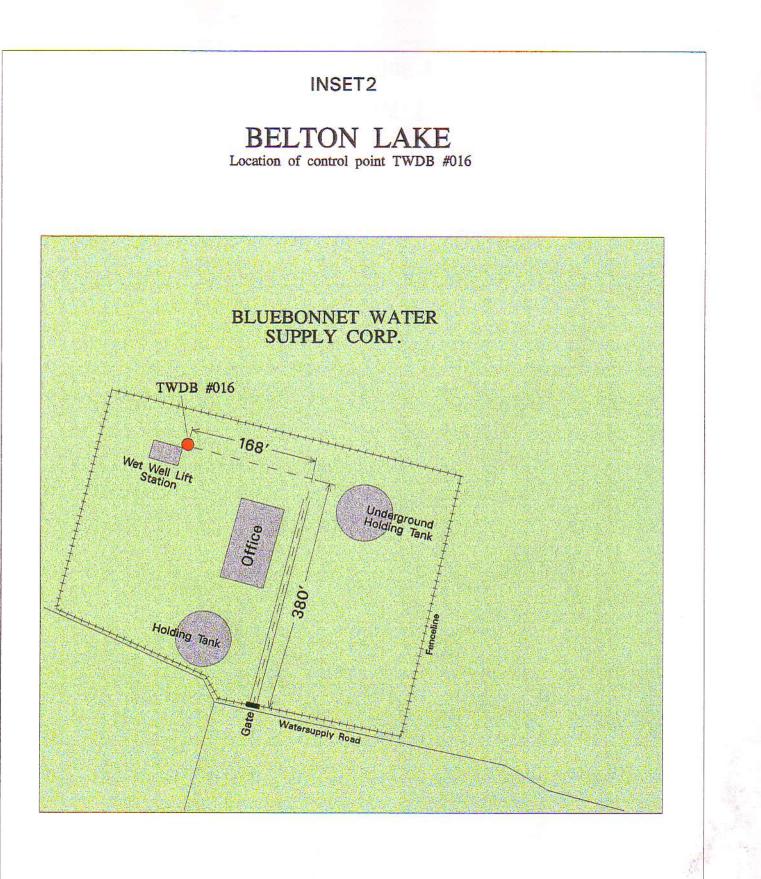
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